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describes the percentage improvement (or degradation) which can be expected for a given new notional fighter/attack aircraft design. The MIM statisti-

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20. ABSTRACT (continued)

ically derives a predicted value for maintenance-manhours-per-flight-hour (MMI/FH) based on prior aircraft performance using design parameters such as vehicle weight or speed. The percentage difference between the statistical prediction and a contractor's submission is the R&M TIF.

This report describes the justification, and the rationale for determining the validity, or the reasonableness, of TIF's presented in a new weapons system design proposal.

UNCLASSIFIED

PREFACE

This report was prepared by the Maintainability Engineering Group of the Vought Corporation, Dallas, Texas under Contract No. N00140-79-C-0445 for Naval Air Systems Command, Washington, D.C. The objective of this study was to address the differences between aircraft maintainability requirements derived from the Maintainability Index Model (MIM) and the aircraft maintainability requirements predicted by a contractor. Methodology for assuring technology improvements and evaluating contractor predictions is discussed.

This project was conducted under the technical cognizance of Messrs.

George J. Donovan and Carl Tanger, Airframe and Equipment Branch, AIR-4114.

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SUMMARY

The Maintainability Index Model (MIM) presented in the Aircraft Maintenance Experience Design Handbook provides a method of measuring predicted mainability technology improvement of a notional system over a baseline of system operational experience and design parameters. The objective of this study was to provide the methodology necessary to validate this predicted technology improvement during the conceptual phase of a system.

The study addresses aircraft maintenance significant areas by system and subsystem, identifying those subsystems in which technology improvement will have the most significant impact on maintenance resources and requirements. The influence of technology, design philosophy, and commonality of systems on maintainability technology improvement also is discussed.

Methodology is provided for a subjective evaluation of predicted maintainability technology improvements in a system. In general, it will verify, with a reasonable degree of certainty, that improvement or lack of improvement that will result from innovations of the system design concept.

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1.1 OBJECTIVE OF STUDY

The objective of this study was to address the differences between aircraft maintenance requirements as determined by the Maintainability Index Model (MIM) and aircraft maintenance requirements as predicted by a contractor during conceptual design. Methodology for assessing technology improvements and evaluating contractor predictions is discussed.

1.2 HISTORICAL BACKGROUND

Under an earlier contract from NAVAIR, reference (1), Vought Corporation developed a model for predicting baseline maintainability characteristics of notional Navy Fighter, Attack, and Anti-Submarine Warfare (ASW) aircraft. The model functionally relates aircraft maintenance characteristics at the two-digit Work Unit Code (WUC) level to aircraft design characteristics. A computer program, reference (2), is used to size the given conceptual aircraft for baseline maintainability requirements. The term baseline maintainability requirements is used to identify the maintenance requirements of an aircraft designed with the technology that existed when the active Navy Fighter/Attack/ASW aircraft were built. When baseline model data is compared with the contractor's maintainability predictions, the amount of technology improvement anticipated for the new generation aircraft can be measured. Units of measurement are maintenance man-hours per flight hour (MMH/FH), maintenance actions per flight hour (MA/FH) and mean time to repair (MTTR) at the Organizational and Intermediate levels of maintenance.

A user of the MIM must be able to relate the measured technology improvement with qualitative design features implemented in the new design. For example, if the model showed a 34% technology improvement in the Flight Controls System MMH/FH, an evaluator would want to know if this value is reasonable and whether the Reliability and Maintainability (R&M) design features stated in a contractor's proposal could result in a 34% reduction in MMH/FH.

1.3 GENERAL APPROACH

The approach taken to satisfy the study objective was to:

- o Identify baseline maintainability requirements as determined by the MIM.
- o Identify the maintenance significant items within a system and rank them by subsystem.
- o Discuss the criteria for evaluating maintainability predictions.

2.0 MIM BASELINE TECHNOLOGY

2.1 MAINTAINABILITY INDEX MODEL

The Maintainability Index Model (MIM) determines baseline maintenance requirements for a given aircraft dependent on that aircraft's design characteristics. Statistical extrapolation of existing trends are used to establish baseline maintenance requirements as measured in maintenance man-hours per flight hour (MMH/FH) and maintenance actions per flight hour (MA/FH). These resultant values reflect some level of R&M effort commensurate to the technology that existed when the data base aircraft were built. This section will address the problem of increased weapon system complexity and equipment commonality on maintainability predictions.

2.2 AIRCRAFT DATA BASE

The aircraft used in the development of the MIM were initially designed to some level of R&M and that effort is reflected in the model data base. Unfortunately, increased weapon system complexity has overshadowed many good R&M features implemented in a design, compounding the problem of technology evaluation. Furthermore, changes in 3-M data over time have added another variable to the problem.

The existing model data base was compiled from Fleet experience of aircraft developed during the late 1960's and early 1970's and operating in the Fleet during the mid 1970's. Since then, maintenance expenditures on the aircraft used to develop the MIM has increased resulting in the model under predicting current year (1979) data by 40% and life cycle average data by 18% (reference 3). This has resulted in a program for updating the MIM on a periodic basis.

2.3 SYSTEM COMPLEXITY

History has shown that the addition of more parts, components, and equipment to a weapons system increases the probability of maintenance after a flight, resulting in higher MMH/FH expenditures. Although new technology has improved component reliability (failures per part per flight hour), it also has permitted an increase in density of functions and capabilities (numbers of parts per subsystem). This point is illustrated by Figure 1 which shows component reliability increasing over time while system reliability is decreasing. This has resulted in an overall increase in aircraft maintenance requirements.

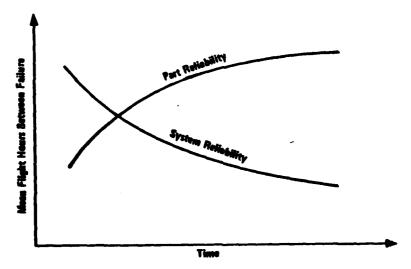


Figure 1. Technology Trends in Aircraft Reliability

The system level maintainability estimating relationships used in the MIM are responsive to this change and are thus useful in sizing a new conceptual aircraft design for baseline maintainability requirements. The primary design parameters affecting the model are aircraft weight, speed, and thrust.

Figure 2 shows how dependent total aircraft MMH/FH is on aircraft avionics weight relative to the year of first fleet delivery.

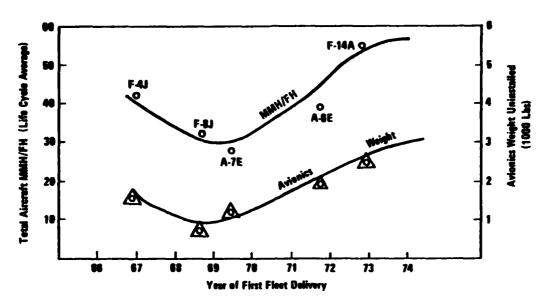


Figure 2. Aircraft Maintenance as a Function of Avionics Weight

Historical data showed that as aircraft avionics weight increased, so did system maintenance. This trend even held true for the newer generation of aircraft (F-14A, S-3A) with improved avionics equipment. One reason for this trend was that advances in design technology were off-set by the addition of more equipment to the aircraft. Consequently, it becomes exceedingly difficult for a new aircraft to show a significant reduction in maintenance and support costs as long as performance and capability increase.

2.4 EFFECTS OF TECHNOLOGY ON MAINTAINABILITY

The MIM was designed to be responsive to advances in design technology and improvements in reliability and maintainability. The model can accept or

measure the net technology improvement predicted over a baseline design depending on input constraints. The problem of how much improvement can be expected for a new design becomes exceedingly difficult to measure because of the variables in the data and the problems of quantifying subjective qualitative design features.

Figure 3 shows a typical relationship between MMH/FH and system complexity as a function of R&M program effort. The customer must determine to what level of effort a program will be funded in order to achieve a specified level of maintainability. The degree of technology improvement implemented in a design is bounded by two curves. The upper curve identifies baseline MMH/FH as determined by the model. The lower curve identifies a theoretical or maximum R&M effort that is still cost effective within the program constraints. Somewhere in between is the optimum level of maintainability to be specified by the customer or predicted by the contractor.

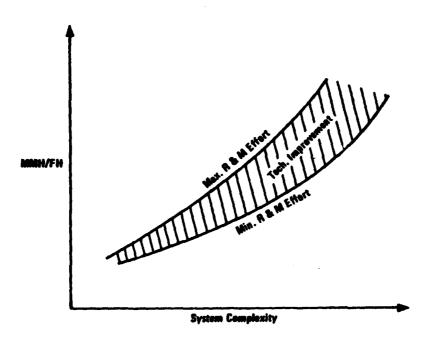


Figure 3. Level of Maintainability Effort

2.5 EQUIPMENT COMMONALITY

A recent report (reference 4) concluded that the most striking characteristic of technology change is its essential continuity across generations of aircraft. The study showed the high commonality of avionics, mission, and support equipment among the A-7, F-4, and F-14 aircraft. Even the newest and most technologically advanced aircraft, the F-14A, was found to have at least 52 percent of its study items incorporated from existing technology on board the A-7 and F-4 aircraft (Table 1). This finding should introduce an element of caution into claims of major manpower reductions for new generations of weapons systems through advanced technology.

TABLE 1. EQUIPMENT COMMONALITY

	A-7B	A-7E	F-4J	F-4N	F-14A
Study Items (165)	71	80	69	64	91
Common to A-7E	55		43	43	42
Common to F-4J	38	43			37
Common to F-14A	34	42	38	63 36	
Common to A-7 and F-4				-	47

Source: Reference 3

3.0 SUBSYSTEM DATA ANALYSIS

This section of the study addresses aircraft maintenance data at the three-digit Standard Work Unit Code (SWUC) subsystem level. The intent of this section is to provide supplemental data to support the two-digit SWUC system analysis defined in the MIM and the five-digit WUC component analysis defined in references (5) and (6).

Appropriate historical maintenance data is included in this section to highlight the problem areas of each system. Data is presented in a bar chart format, ranking those subsystems which contribute the most maintenance to each system. It is hoped that by identifying the maintenance significant subsystems of existing aircraft, steps can be taken to correct or minimize future maintenance problems on the next generation of aircraft.

For each system, two sets of bar graphs are presented. The first depicts a subsystem ranking by MMH/FH and MA/FH for a typical aircraft that is most representative of the given system. The second illustration shows average repair time by type aircraft for the high maintenance subsystems. Mean values are presented for both Organizational (0) and Intermediate (I) levels of repair. A brief narrative description commenting on data behavior and qualitative maintainability features is also included. For a more detailed discussion of qualitative maintainability assessment of individual items, see references (1), (5), and (6).

The data base for this study is the same one that was used in the development of the MIM. Raw 3-M data tapes from the 1975/1976 time period were processed by Vought computer routines resulting in a Standard Work Unit Code

Summary Report. Excerpts from this report are presented as Appendices A and B with an aircraft WUC to SWUC Matrix presented in Appendix C.

3.1 SWUC 11/12 AIRFRAME/FUSELAGE SYSTEMS

The Airframe/Fuselage Systems accounts for approximately 9% of the total average unscheduled maintenance man-hours expended on the study aircraft. A typical distribution of Airframe/Fuselage Systems maintenance is shown in Figure 4. The graph, based on A-6E data, shows the Structures Subsystem to have the largest maintenance expenditure with 57% of the man-hours and 49% of the maintenance actions. The Access Doors/Panels Subsystem also is noted as a major contributor because it accounts for an additional 25% of the maintenance actions expended against the system. In all cases the level of maintenance is predominately Organizational. The average repair times for the two major subsystems are illustrated in Figure 5 for the eight study aircraft. On-aircraft (0-level) repair times were generally reasonable except for the AV-8A expenditure in the Structure Subsystem which was twice the mean time of 3.6 hours. Structural repairs to the A-7E and F-14A Wing Outer Panel Skin account for the higher than normal I-level repair times. Repairs to the engine removal door on the A-7E accounts for the 28.0 hours repair time in the Access Doors/Panels Subsystem.

One reason for the high repair time at 0-level for the AV-8A Structural Subsystem is the remove and replace requirements for the radome. On the AV-8A aircraft, pitot static lines must be disconnected, several access panels must be removed, and a reaction nozzle must be displaced to allow sufficient clearance for removal. The physical size of the radome by necessity adds to the Elapsed Maintenance Time per Maintenance Action and number of personnel required.

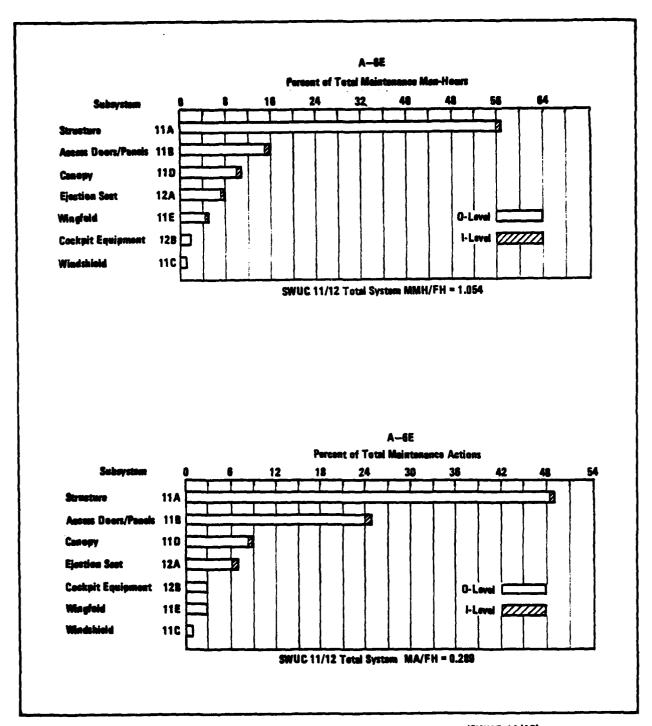


Figure 4. Distribution of A-6E Airframe/Fuselage Systems Maintenance (SWUC 11/12)

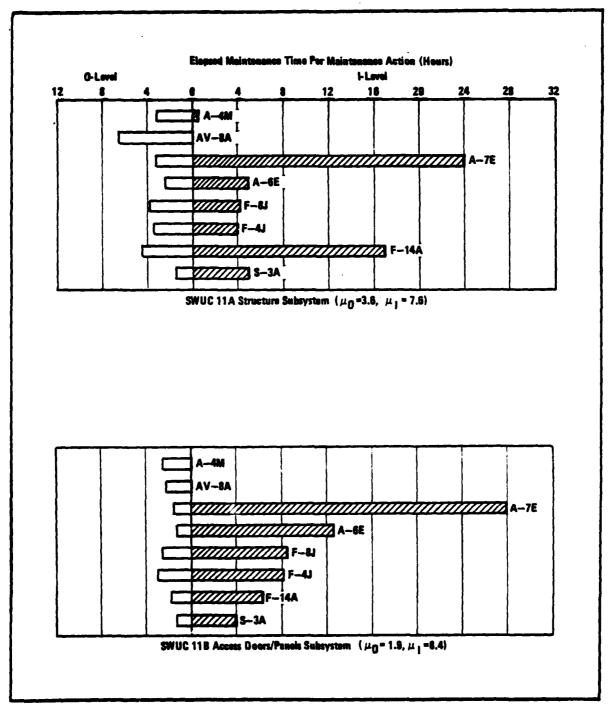


Figure 5. Average Repair Time for Major Airframe/Fuselage Subsystems (SWUC 11/12)

3.2 SWUC 13 LANDING GEAR SYSTEM

The Landing Gear System accounts for about 10% of an aircraft's unscheduled maintenance expenditure as measured in MMH/FH. Figure 6 shows a typical distribution of Landing Gear System maintenance using F-14A data. Within this system, the Wheel/Tire Assembly, Main Landing Gear (MLG) and Doors Subsystem and the Brake Subsystem account for 67% of the manhours expended and 74% of the maintenance actions reported.

The majority of the F-14A Wheel/Tire Assembly maintenance is done at I-level where an average repair time of 3.8 hours is almost twice the mean value for all eight aircraft as shown in Figure 7. On-aircraft repair for most aircraft is less than one hour but ranges from 1.1 to 3.8 hours at I-level. Similar distributions of repair time at 0 and I-levels for the MLG and Doors Subsystem and the Brake Subsystem show wide ranges in average repair time.

The degree of technology improvement predicted in a new aircraft's Landing Gear System should be a function of the R&M effort made in the above three subsystems.

A positive maintainability feature noted during the study was in the Main Landing Gear Wheel and Tire Subsystem on the S-3A aircraft. A special bolt is used, which when tightened, keeps the brake discs aligned while the tire is off. This feature eliminates one of the time consuming installation steps - brake disc alignment. This is a prominent contributing factor to the low average Elapsed Maintenance Time per Maintenance Action shown in Figure 7 (SWUC 13C for O-level maintenance) on the S-3A aircraft.

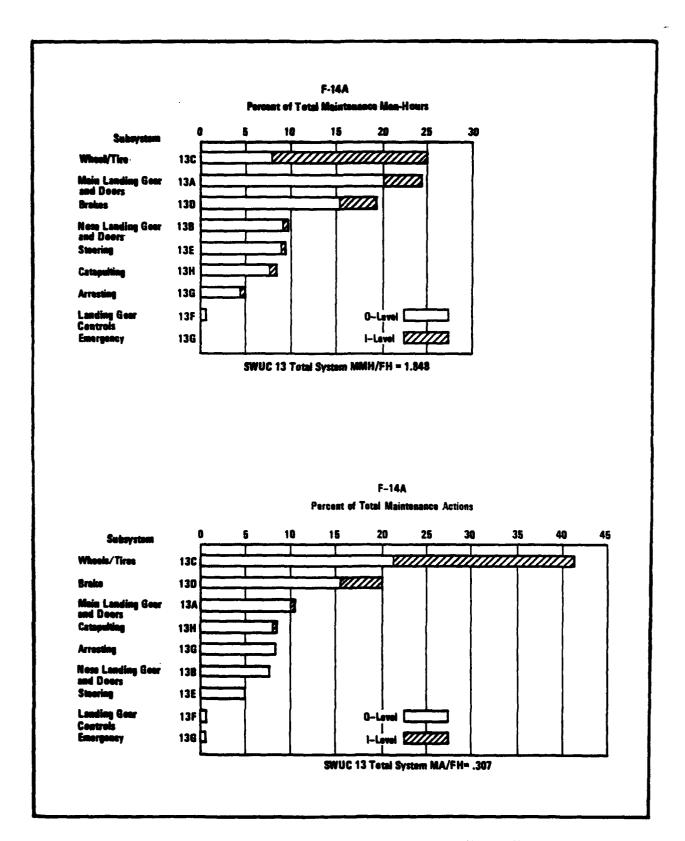


Figure 6. Distribution of F-14A Landing Gear System Maintenance (SWUC 13)

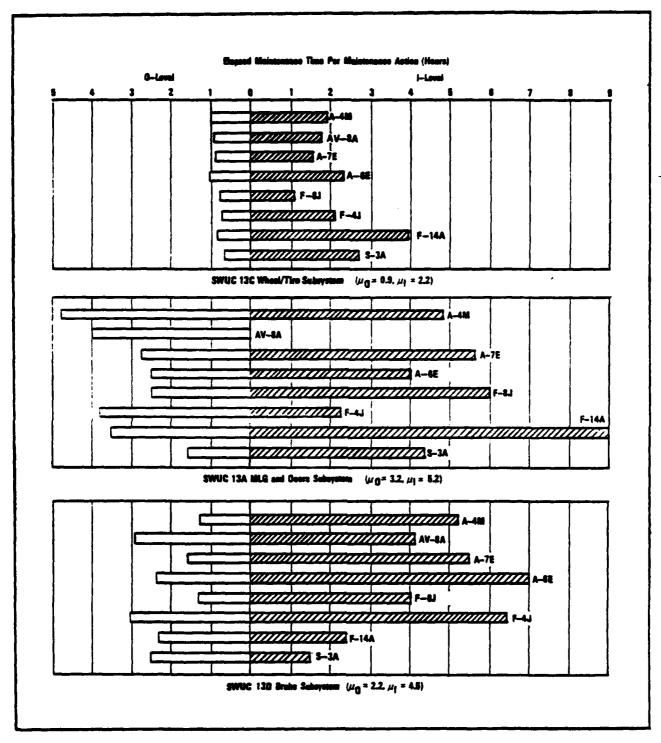


Figure 7. Average Repair Time of Major Landing Goor Subsystems (SWUC 13)

A negative maintainability feature noted in the Brake Subsystem was the use of shims and sealant during installation of the brake on the F-4J aircraft. As noted in Figure 7 (SWUC 13D), the average elapsed maintenance time for O-level maintenance is the highest of all study aircraft.

An installation utilizing a tripod type main landing gear design appear to be less costly to maintain. For example, the use of this type installation allows for removal and replacement of components such as a shock strut without removal of the wheels and tires. In addition; the use of tripod gears requires a smaller and lighter shock strut.

3.3 SWUC 14 FLIGHT CONTROLS SYSTEM

The Flight Controls System contributes about 7% of the total average unscheduled maintenance time expended on the eight study aircraft.

The maintenance distribution of the Flight Controls System is presented in Figure 8 using F-4J data as the representative aircraft. Three of these subsystems, Flaps/Slats, Lateral Control, and Longitudinal Control, account for 84% of the man-hours and 80% of the maintenance actions reported against the system.

Figure 9 depicts the average repair times for the three subsystems for each of the eight study aircraft. The F-4J falls close to the mean time for each of the subsystems and represents an almost even distribution of 0 and I-level maintenance time. This is not the case with the F-14A which depicts an average repair time of twice the mean time for the Lateral Control Subsystems in both I and O-level maintenance. Similar excursions are noted for the other subsystems and for other aircraft.

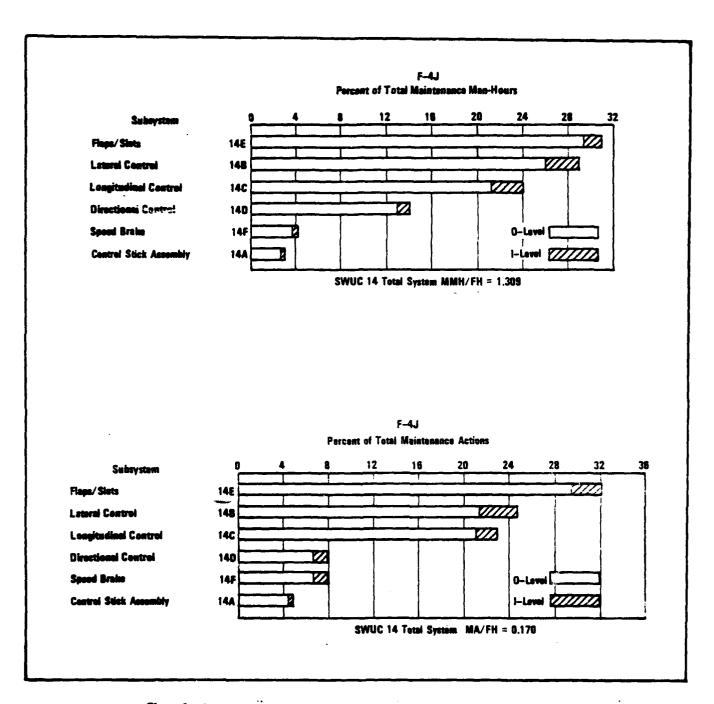


Figure 8. Distribution of F-4J Flight Controls System Maintenance (SWUC 14)



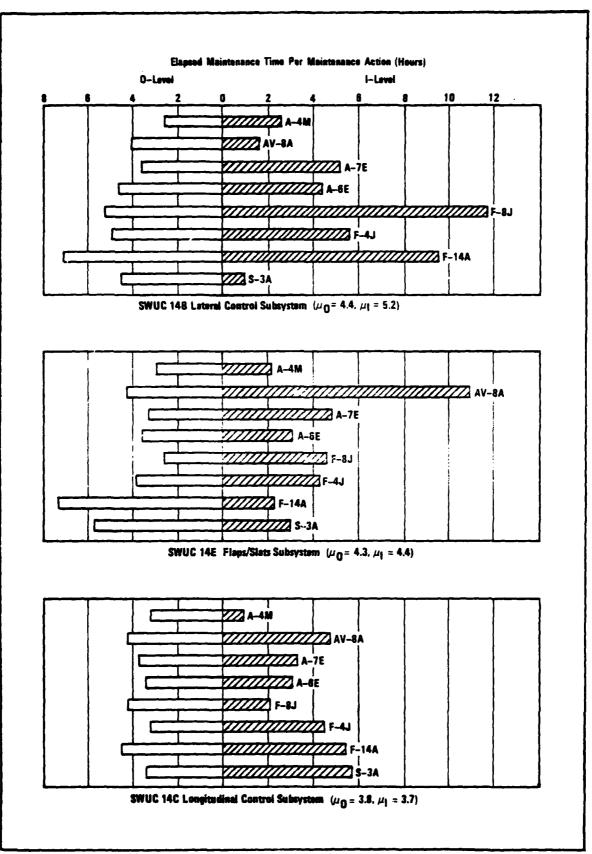


Figure 9. Average Repair Time for Major Flight Controls Subsystems (SWUC 14)

Negative maintainability features noted in the Flight Controls System were inadequate hand/tool room for repair action, requirements for rigging after repair, and the number of fastener removals required for access.

3.4 SWUC 23 ENGINE SYSTEM

The Engine System averages about 9% of the unscheduled maintenance generated by the eight study aircraft. Figure 10 presents a typical distribution of Engine System maintenance using S-3A data. The distribution indicates the basic Engine and the Main/AB Fuel subsystem to be the two major engine subsystems accounting for 85% of the man-hours and 68% of the maintenance actions expended.

The average repair times for the two major subsystems are presented in Figure 11 for comparison of expenditures between the eight study aircraft. The average repair times for the Basic Engine System are at 8.4 and 7.9 hours for 0 and I-levels respectively. Organizational level repair time is primarily a function of engine removal and replacement time. As a typical aircraft, the S-3A falls within the mean limits, but the F-14A sets the maximum I-level expenditure of 12.4 hours and the A-7E shows a 12.6 hour rate for 0-level maintenance. Similar distributions are shown for the Main/AB Fuel Subsystem although lesser in magnitude and more predominantly 0-level expenditures.

3.5 SWUC 29 POWER PLANT INSTALLATION SYSTEM

Only about 2% of the total average unscheduled maintenance time is attributed to the Power Plant Installation System. Using A-6E data, Figure 12 was derived to show a typical distribution of Power Plant Installation System maintenance. The data shows the Exhaust Subsystem and Power Plant Controls Subsystems accounted for 84% of the man-hours and 74% of the maintenance actions reported against the system.

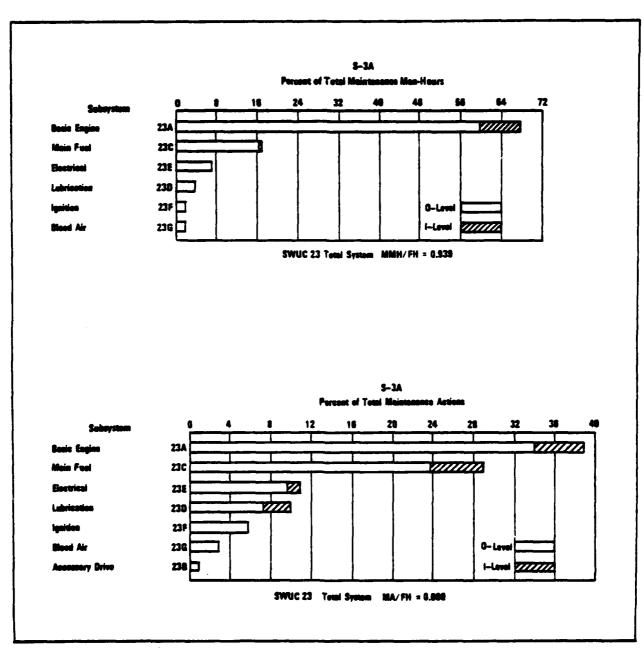


Figure 18. Distribution of S-3A Engine System Maintenance (SWUC 23)

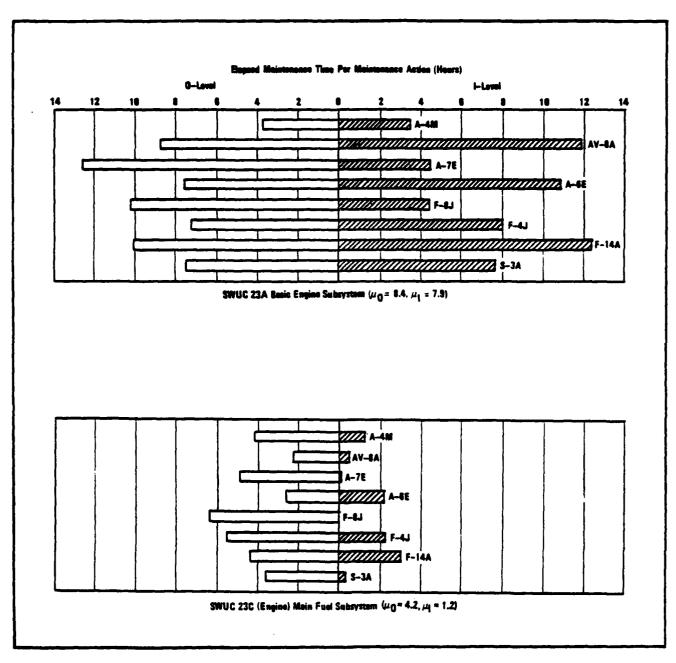


Figure 11. Average Repair Time for Major Engine Subsystems (SWUC 23)

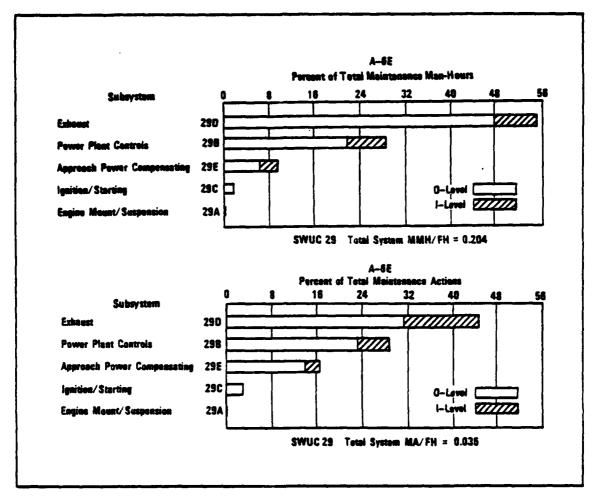


Figure 12. Distribution of A-6E Power Plant Installation System Maintenance (SWUC 29)

The majority of the A-6E Exhaust Subsystem maintenance is performed on-aircraft where an average repair time of 3.6 hours is almost 28% greater than the mean time for all the reporting aircraft as shown in Figure 13. At I-level the A-6E repair time is equivalent to the mean of 2.5 hours where I-level repair ranges from 1.2 to 6.6 hours. Similar 0 and I-level mean times are noted for the Power Plant Controls Subsystem with a comparable range of repair times.

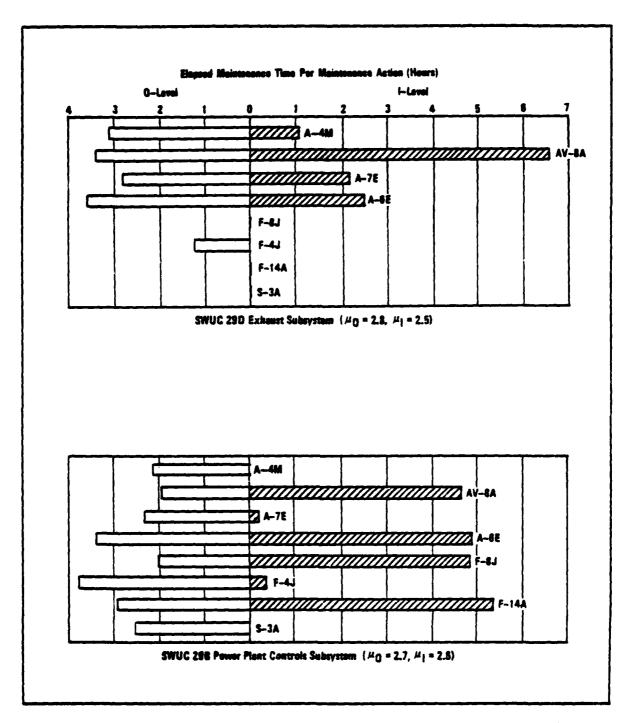


Figure 13. Average Repair Time for Major Power Plant Installation Subsystems (SWUC 29)

3.6 SWUC 41 AIR CONDITIONING SYSTEM

On the average about 2% of the total unscheduled maintenance time expended on each of the study aircraft was attributed to the Air Conditioning System. Figure 14 shows a typical distribution of Air Conditioning System maintenance using F-14A data. Within this system the Air Conditioning and Pressurization Subsystems account for 66% of the man-hours expended and 61% of the maintenance actions reported.

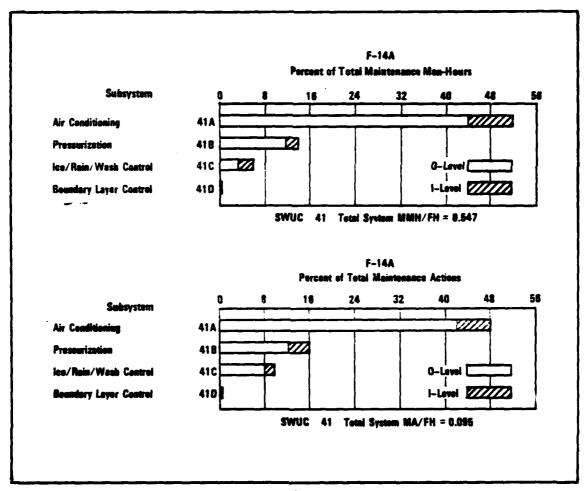


Figure 14. Distribution of F-14A Air Conditioning System Maintenance (SWUC 41)

The majority of the F-14A Air Conditioning Subystem maintenance is done at 0-level where an average repair time of 3.5 hours is slightly over the mean value of all eight study aircraft as shown in Figure 15. The I-level repair times range from 0.6 to 2.8 hours with the F-14A showing an average repair time slightly more than half the mean value of 1.7 hours. Similar distribution of repair times are shown for the Pressurization Subsystem at 0 and I-levels with a wider distribution of repair times from 0.5 to 5.6 hours noted in the I-level expenditures.

A negative maintainability feature noted in this system during the study was the maintenance requirements for the AV-8A Temperature Controller which has hard-wired switches. Maintenance on these switches requires unsoldering, soldering, unpotting, and potting electrical connections in the cockpit or cutting and later splicing wires. These requirements are not only undesirable, they also are very time consuming (see Figure 15, SWUC 41A, O-level for the AV-8A aircraft).

3.7 SWUC 42 ELECTRICAL SYSTEM

The unscheduled maintenance expenditures attributed to the Electrical System amounts to about 6% of the total average time expended on each of the study aircraft. Data from the F-4J was used to produce the typical distribution of Electrical System maintenance shown in Figure 16. Within this system the AC Power Supply and Aircraft Wiring Subsystems account for 73% of the manhours expended and 72% of the maintenance actions reported.

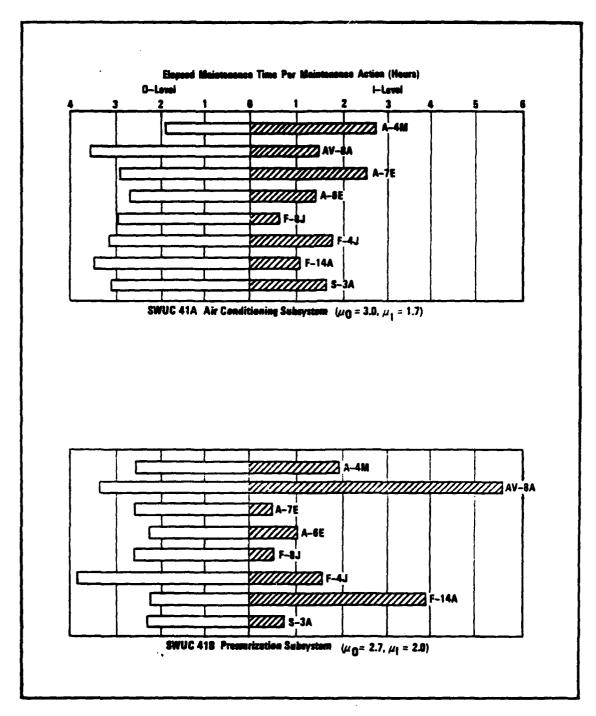


Figure 15. Average Repair Time for Major Air Conditioning Subsystems (SWUC 41)

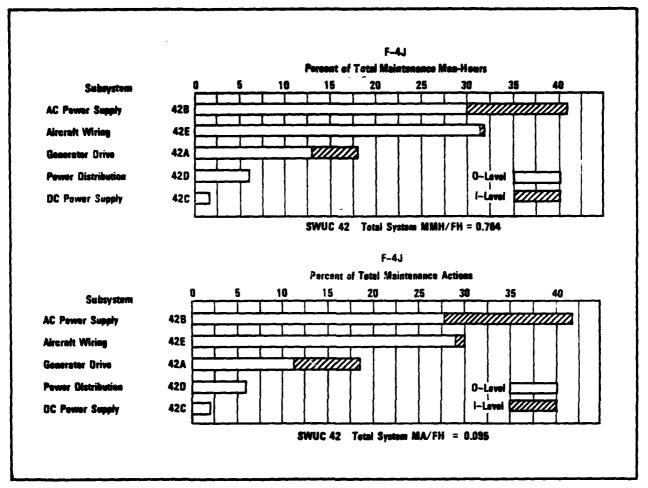


Figure 16. Distribution of F-4J Electrical System Maintenance (SWUC 42)

Figure 17 depicts the average repair times for the three major subsystems for each of the study aircraft. For the AC Power Supply Subsystem the F-4J represents an almost even distribution of maintenance level repair times with an expenditure of about 1.2 hours over the mean value. Repair actions against the Generator Regulator Panel and Generator are the contributing factors. For the aircraft Wiring Subsystem the I-level repair time for the F-4J is over three times the mean value and represents the widest excursion within the

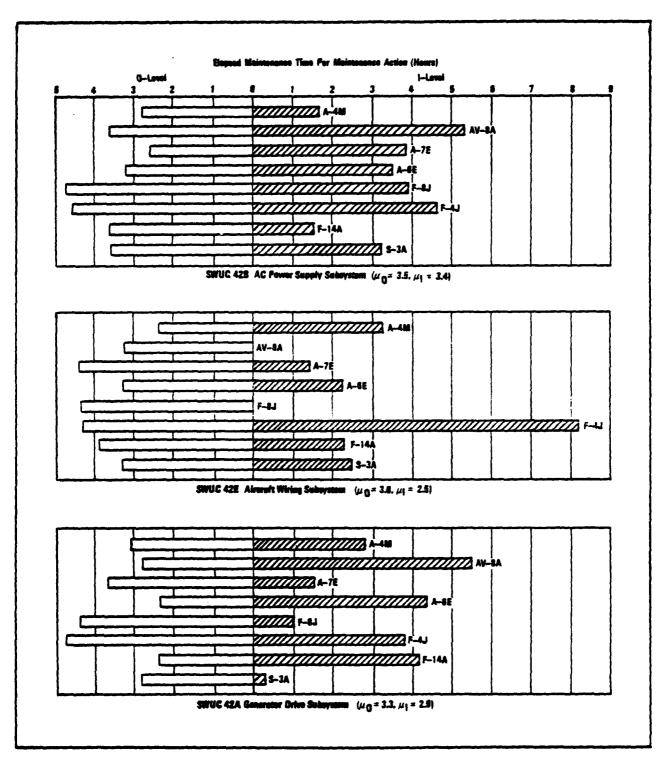


Figure 17. Average Repair Time for Major Electrical Subsystems (SWUC 42)

study aircraft. Anomalies related to the wiring circuits for the Fire Detection, Exterior Lighting, and Engine Start Subsystems are the drivers in repair time. A closer time distribution is noted in 0-level. Similar repair time distribution is shown for the Generator Drive Subsystem.

A negative maintainability requirement noted in the Electrical System was the requirement, in many instances, for an engine run to operationally check a component after installation. For example, after removal and replacement of the Generator Control Panel on the F-8J aircraft, an engine run is required to operationally check the Electrical System. This requirement has an influence on the Elapsed Maintenance Time per Maintenance Action (see Figure 17, SWUC 42B, O-level).

3.8 SWUC 44 LIGHTING SYSTEM

The Lighting System contributes about 2% of the unscheduled maintenance time expended on each of the study aircraft. F-8J data was used to show a typical distribution of Lighting System maintenance (Figure 18).

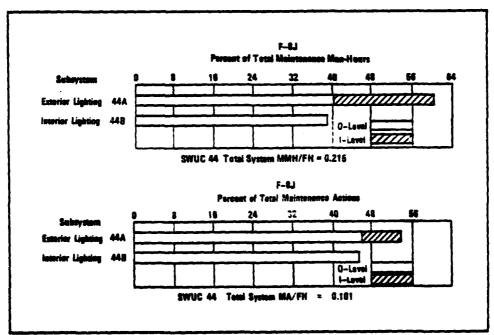


Figure 18. Distribution of F-8J Lighting System Maintenance (SWUC 44)

This system is comprised of two subsystems, Exterior and Interior Lighting, with the Exterior Subsystem accounting for 61% of the man-hours expended and 54% of the maintenance actions reported. The majority of the F-8J Exterior Lighting maintenance is performed at I-level where an average repair time of 3.7 hours is substantially over the mean value of 2.9 hours for all eight study aircraft shown in Figure 19. On-aircraft repair times range from 1.1 to 1.7 hours resulting in a mean of 1.3 hours which corresponds to the repair time for the typical aircraft. Similar distributions are noted for the Interior Lighting Subsystem for both maintenance levels. The mean repair time for the I-level is 3.6 hours because of a large increase in expenditures on the F-14A.

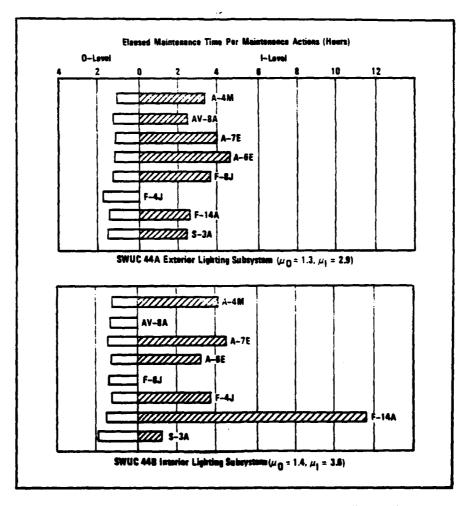


Figure 19. Average Repair Time for Major Lighting Subsystems (SWUC 44)

The negative maintainability features noted in this system were primarily the requirement to remove panels which have numerous screws to gain repair access. For example, to repair the Tail Position Lights on the F-4J aircraft an access panel with 40 screws must be removed. Support for this type design is what drives the Elapsed Maintenance Time per Maintenance Action (see Figure 19, SWUC 44A, O-level for the F-4J aircraft).

3.9 SWUC 45 HYDRAULIC SYSTEM

The Hydraulic System was found to contribute only about 3% of the unscheduled maintenance time expended on the study aircraft. A typical distribution of Hydraulic System maintenance is shown in Figure 20. The graph, based on A-7E data, shows that the Normal Hydraulic Subsystem accounts for the largest maintenance expenditure with 73% of the man-hours and 74% of the maintenance actions reported.

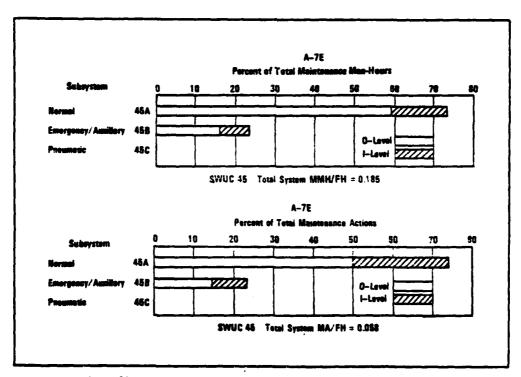


Figure 20. Distribution of A-7E Hydraulic System Maintenance (SWUC 45)

In Figure 21 the average repair times for the major subsystems is presented for the eight study aircraft. The A-7E shows the least repair time expenditure and averages 40% less time than the mean time of 3.1 and 3.2 expended by the eight aircraft for 0 and I-levels respectively. On-aircraft repair times range from 2.1 to 3.9 hours while the I-level, because of an extreme repair time expenditure for the F-14A ranges from 1.8 to 8.3 hours.

The high Elapsed Maintenance Time at O-level for the AV-8A aircraft is influenced by the requirement to remove the Wing to gain access to the Hydraulic Reservoir for adjustment and/or repairs (see Figure 21, SWUC 45B).

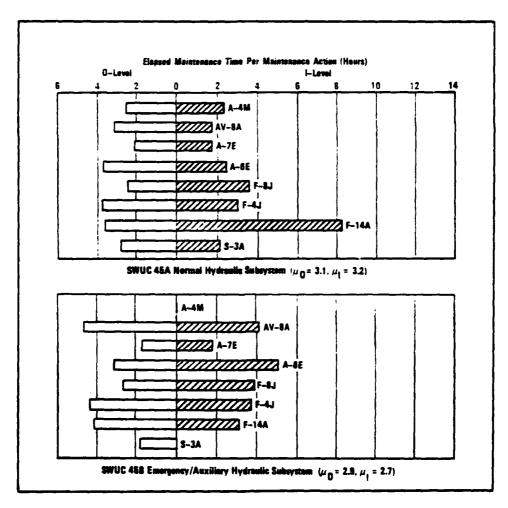


Figure 21. Average Repair Time for Major Hydraulic Subsystems (SWUC 45)

3.10 SWUC 46 FUEL SYSTEM

About 3% of the unscheduled maintenance expended on the eight study air-craft was attributed to the Fuel System. Figure 22 shows a typical distribution of Fuel System maintenance using A-6E data. It indicates that the Internal Fuel Subsystem is the major contributor accounting for 67% of the man-hours expended and 57% of the maintenance actions reported.

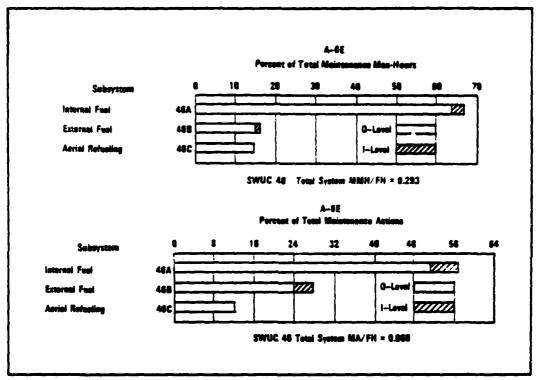


Figure 22. Distribution of A-SE Fuel System Maintenance (SWUC 46)

A comparison plot is shown in Figure 23 for the average repair time expended on the Internal Fuel Subsystem for each of eight study aircraft. The majority of the repair time is performed at 0-level with the A-6E reporting an expenditure of 2.8 hours. This is substantially less than the mean value of 4.1 hours for the reporting aircraft which range from 2.3 to 7.0 hours. A similar distribution of lesser magnitude is noted at I-level where a mean repair time of 1.2 hours was noted based on a range of 0 to 2.7 hours.

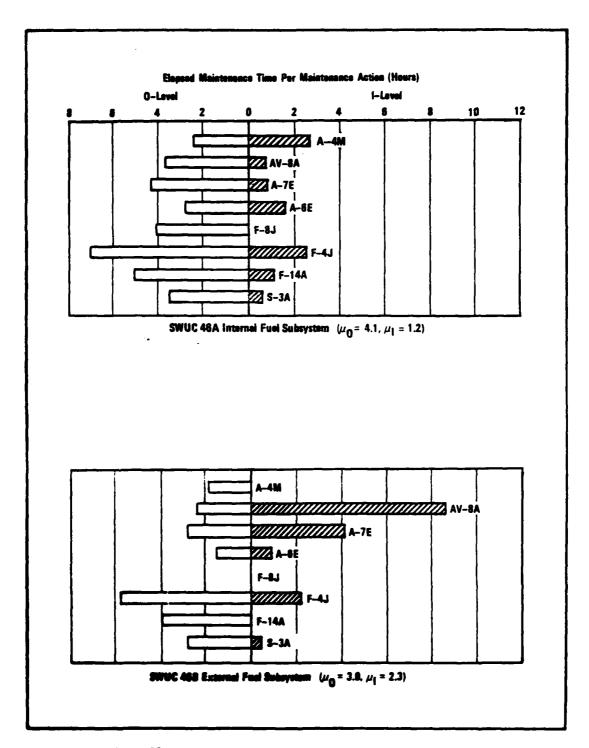


Figure 23. Average Repair Time for Major Fuel Subsystems (SWUC 46)

3.11 SWUC 49 MISCELLANEOUS UTILITIES SYSTEM

As an unscheduled maintenance time contributor the Miscellaneous Utilities System accounts for less than 1% of the total time attributed to each of the study aircraft. In Figure 24 a typical distribution of Miscellaneous Utilities System maintenance is presented based on F-14A data. Within this system, Fire Detection Subsystem maintenance is performed predominantly at the on-aircraft level.

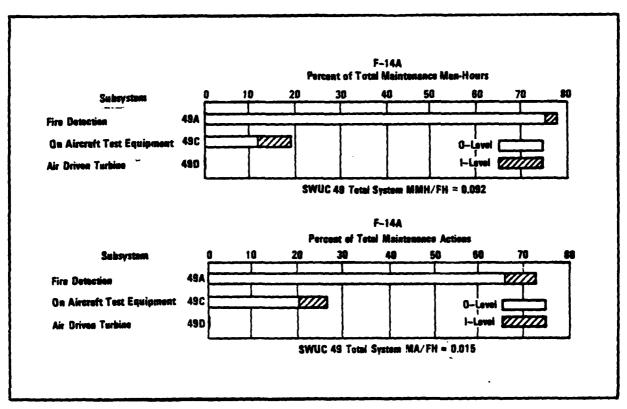


Figure 24. Distribution of F-14A Miscellaneous Utilities System Maintenance (SWUC 49)

The F-14A average repair time is 3.5 hours, slightly exceeding the mean time of 3.0 hours for the eight study aircraft shown in Figure 25. Intermediate level maintenance has a mean repair time of 2.1 hours. This value is somewhat influenced by the relatively large repair time of 12.5 hours reported on the A-4M aircraft. Repair time ranging for the balance of the study aircraft is 0 to 2.1 hours.

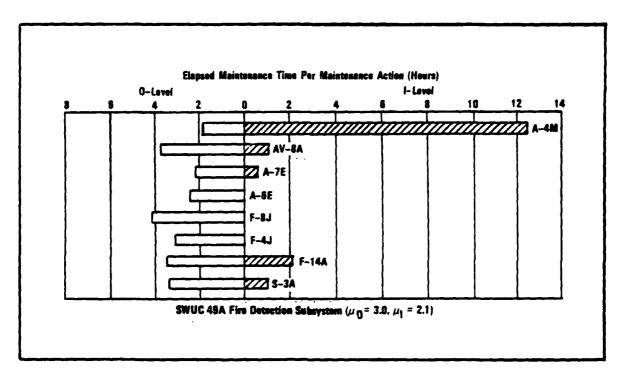


Figure 25. Average Repair Time for Major Miscellaneous Utilities Subsystem (SWUC 49)

3.12 SWUC 51 INSTRUMENT SYSTEM

The Instrument System contributes about 5% of the unscheduled maintenance time expended on the study aircraft. Figure 26 shows a typical distribution of Instrument System maintenance using A-4M data. Within this system three major subsystems, Flight/Navigation Instruments, Fuel Quantity Indication, and Position Indication, account for 72% of the man-hours expended and 77% of the maintenance actions reported.

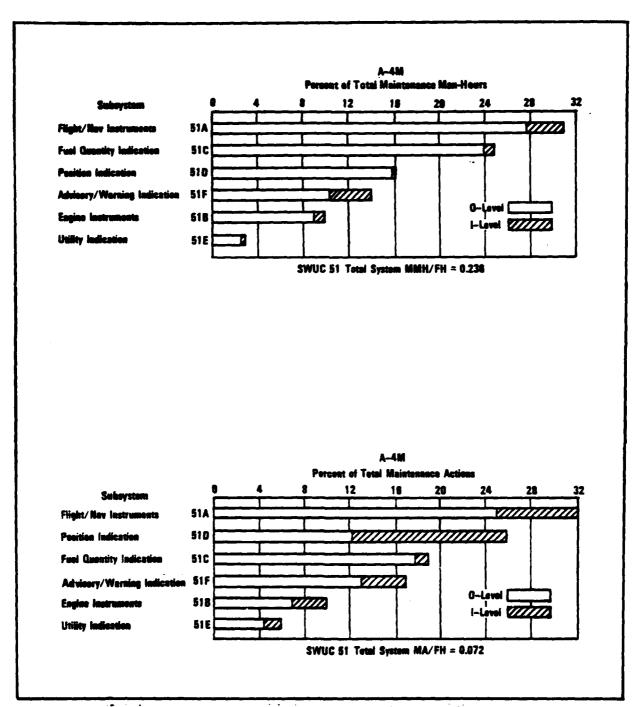


Figure 28. Distribution of A-4M Instrument System Maintenance (SWUC 51)

Figure 27 depicts the average repair times for the three subsystems for each of the eight study aircraft. In each case the majority of the repair time is performed at 0-level. For the Flight/Navigation Instruments Subsystem repair time expenditures are stable with individual aircraft averages generally falling within an hour of the mean repair times of 1.8 and 1.4 hours for 0 and I-level respectively. Wider distributions of repair times are noted for the Fuel Quantity Indication and Position Indication Subsystems at 0 and I-levels with the widest range of repair times resulting from the Fuel Quantity Indicating Subsystem.

A negative maintainability feature noted in the Instrument System for the F-4J aircraft was the requirement to adjust and calibrate the fuel quantity indicators to the fuel probes prior to securing the indicator in the aircraft. This requirement has a significant impact on the Elapsed Maintenance Time per Maintenance Action (see Figure 27, SWUC 51C, O-level maintenance).

3.13 SWUC 56 FLIGHT REFERENCE SYSTEM

The Flight Reference System accounts for 1 to 5% of the total unscheduled maintenance (MMH/FH) expended on each of the eight study aircraft. Using A-4M data, a typical distribution of Flight Reference System maintenance is shown in Figure 28. The Angle-of-Attack Indication (AOA) and Air Data Computer Subsystems are shown as the major maintenance contributors accounting for 76% of the man-hours and 83% of the maintenance actions expended to support the system.

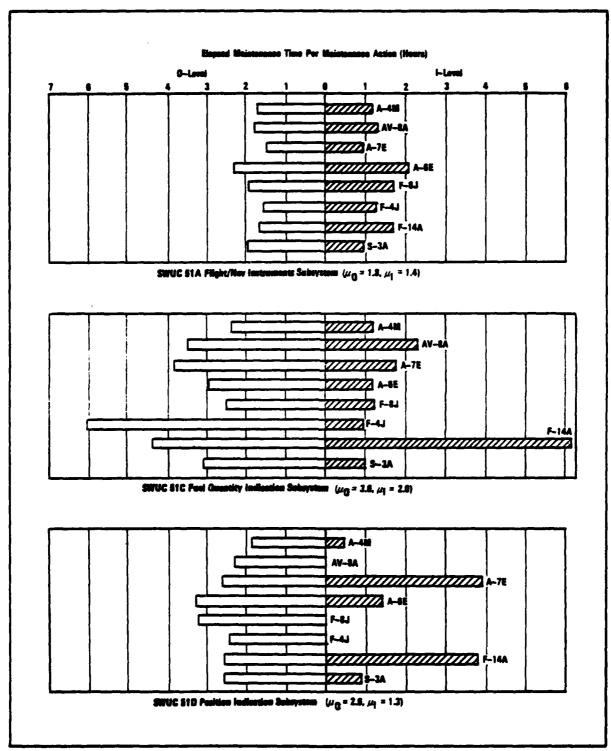


Figure 27. Average Repair Time for Major Instrument Subsystems (SWUC 51)

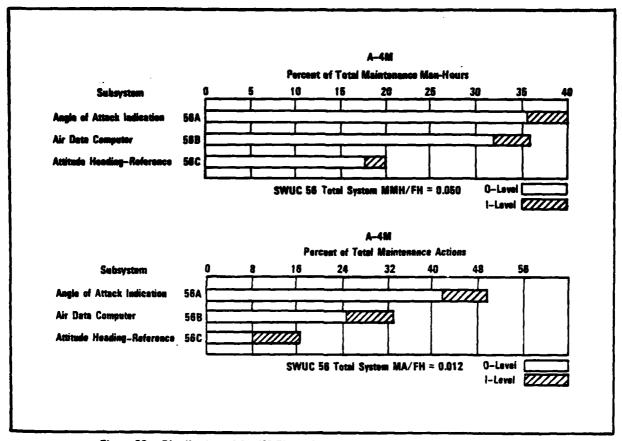


Figure 28. Distribution of A-4M Flight Reference System Maintenance (SWUC 56)

In Figure 29 the average repair times for the contributing subsystems is illustrated for the eight study aircraft. Organizational level maintenance time for the AOA Indication Subsystem is stable about the mean of 1.8 hours. A much wider dispersion of repair times is noted for I-level where the F-14A with a five hour repair time is two and one-half times the mean of the eight aircraft. On-aircraft repair for the Air Data Computer Subsystem is similarly stable about the mean repair time of 1.9 hours for the eight aircraft. The increased complexity of I-level repair is evident in the average times for the AV-8A and F-14A being reported as 10.2 and 11.5 hours respectively against a mean time for all eight aircraft of 6.5 hours.

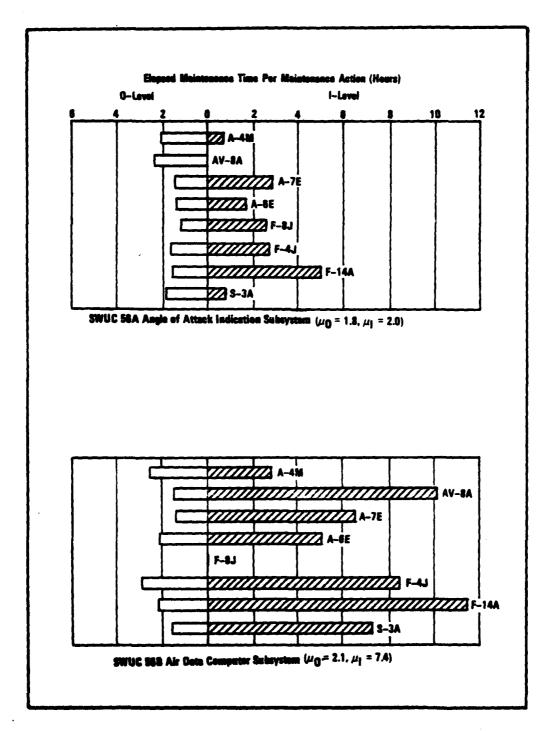


Figure 29. Average Repair Time for Major Flight Reference Subsystems (SWUC 56)

A negative maintainability feature noted in this system was the requirement for removal and replacement of the Angle-of-Attack Transducer in the AV-8A aircraft. To gain access, a panel secured by 14 screws must be removed, wire bundle tie wraps must be cut and subsequently replaced, and even with the panel removed, there is marginal accessibility to the four mounting bolts and electrical connectors. Requirements of this type are what causes increased Elapsed Maintenance Time per Maintenance Action (see Figure 29, SWUC 56A, O-level maintenance). Another negative maintainability feature was noted on the F-4J aircraft where, in order to remove the Air Data Computer, the Ejection Seat and a Receiver-Transmitter (RT) Unit (radio) must be removed (see Figure 29, SWUC 56B, O-level maintenance).

3.14 SWUC 60 COMMUNICATIONS SYSTEM

The Communications System accounts for 4 to 7% of the total unscheduled maintenance (MMH/FH) expended on the eight study aircraft. A typical distribution of communications maintenance based on F-4J data is shown in Figure 30. Of the subsystems listed, the UHF Communications and IFF are the major maintenance consumers accounting for 82% of the man-hours and 75% of the maintenance actions expended. Figure 31 offers a breakdown of the average repair times for each of the eight study aircraft as it pertains to the two major subsystems. On-aircraft repair times (0-level) for both subsystems have some variation but are generally consistent with the mean value of 1.4 and 1.5 hours for the UHF and IFF respectively. The increased complexity of I-level repair is denoted by an increase in the mean repair times to 4.5 and 3.9 hours respectively for these same subsystems. A significantly greater average repair time also is noted for the A-6E and F-4J UHF Communications Subsystem.

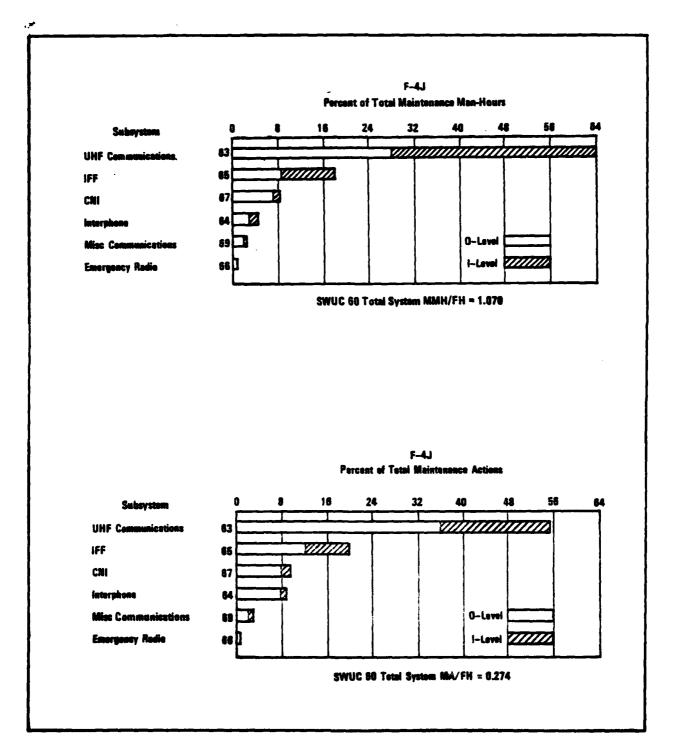


Figure 30. Distribution of F-4J Communications System Maintenance (SWUC 60)

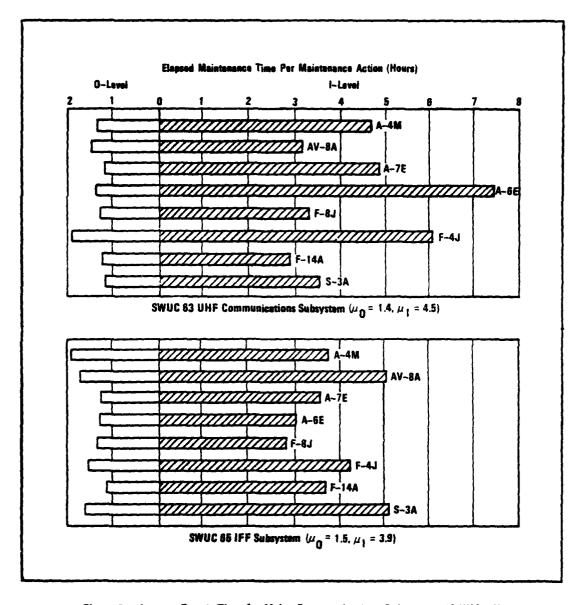


Figure 31. Average Repair Time for Major Communications Subsystems (SWUC 60)

As noted in Figure 31, SWUC 63, O-level, the F-4J indicates a much higher Elapsed Maintenance Time (EMT) per Maintenance Action (MA) than the other aircraft in the study. One reason for the higher EMT/MA is the requirement to remove the Ejection Seat to gain access to the UHF Radio Receiver Transmitter.

3.15 SWUC 71/72/73/74 NAVIGATION/WEAPON CONTROL SYSTEMS

The Navigation/Weapon Control Systems accounted for 16 to 35% of the total unscheduled maintenance (MMH/FH) reported on each study aircraft. Figure 32 shows a typical distribution of subsystem maintenance based on A-7E data. The maintenance requirements are almost equally divided between 0 and I-level for this control grouping. The top three subsystems, Inertial Nav, Radar Set and Miscellaneous Set/Group, are the major maintenance contributors accounting for 51% of the man-hours and 43% of the maintenance actions expended.

A breakdown of the average repair times for each of the eight study aircraft for the three major maintenance contributors is shown in Figure 33. Because of the large grouping of subsystems in the Navigation/Weapon Control area, only some of the aircraft have repair time expenditures for the major subsystems. The A-7E is the only study aircraft with repair times for all three of the major subsystems. No significant deviations are noted in 0 and I-level repair times except for the F-8J where the I-level Miscellaneous Set/Group expenditure of about 11 hours is almost twice the A-7E time.

The primary negative maintainability features noted in these subsystems were the lack of Built-In-Test/Built-In-Test-Equipment (BIT/BITE) provisions for repair verification, lack of rack and panel connectors, equipment located at a level which require the use of a maintenance stand for repair, and the lack of quick release fasteners or latches on panels which require removal for access. For example, 41 stress fasteners must be removed from one panel to gain access to the Radar Altimeter RT Unit on the F-4J aircraft.

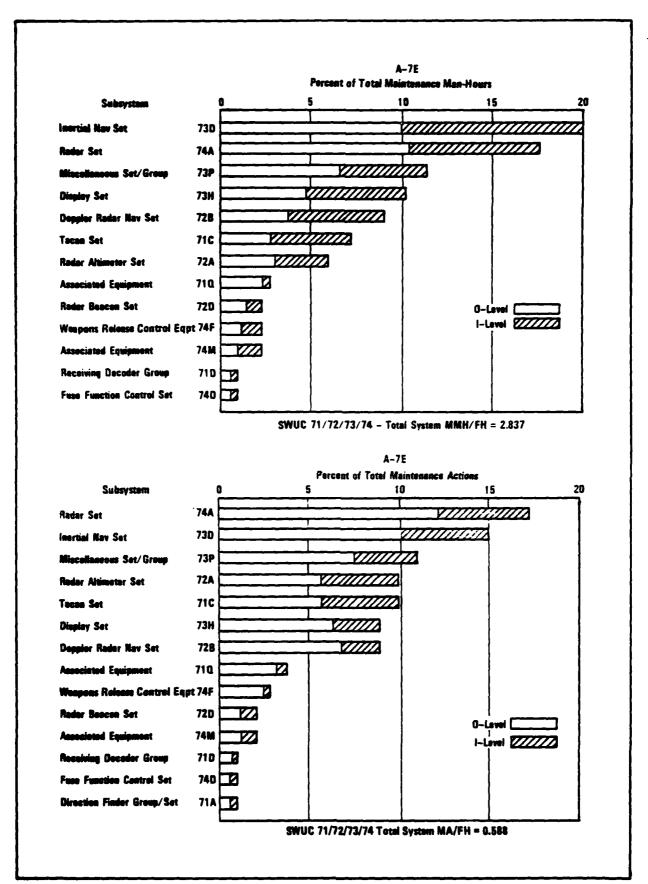


Figure 32. Distribution of A-7E Navigation/Weapon Control System Maintenance (SWUC 71/72/73/74)

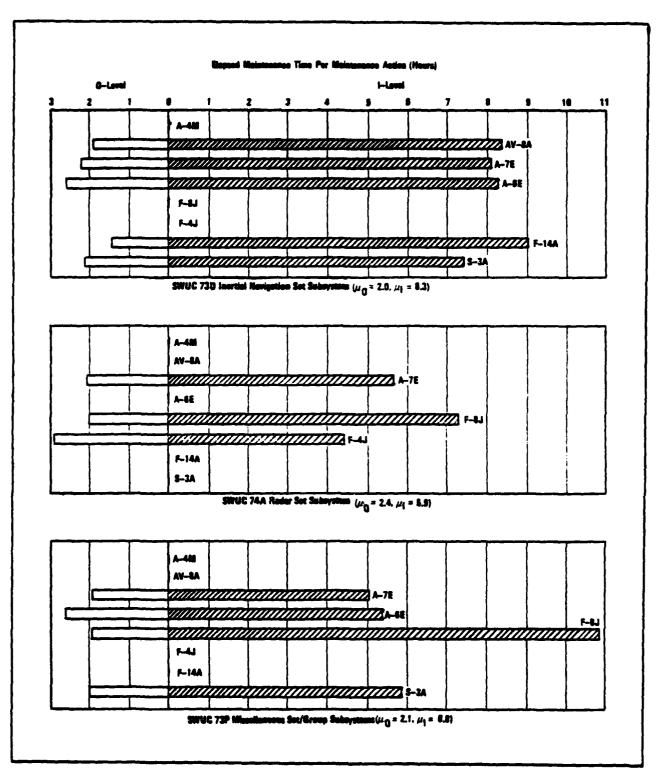


Figure 33. Average Repair Time for Major Navigation/Weepon Control Subsystems (SWUC 71/72/73/74)

3.16 SWUC 75 WEAPONS DELIVERY SYSTEM

The Weapons Delivery System accounts for almost 4% of the total unscheduled maintenance (MMH/FH) reported on the eight study aircraft. A typical distribution of Weapons Delivery System maintenance based on A-7E data is shown in Figure 34. Of the subsystems comprising this system, the Launcher/Racks/Rails is the major maintenance contributor accounting for 63% of the maintenance man-hours expended and 61% of the maintenance actions reported. Man-hour expenditures are almost equally divided between 0 and I-level maintenance categories.

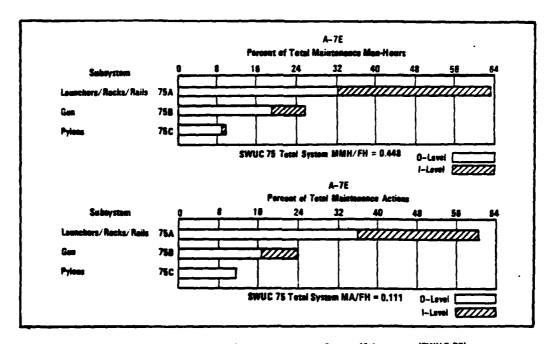


Figure 34. Distribution of A-7E Weapons Delivery System Maintenance (SWUC 75)

In Figure 35 a breakdown of the average repair times associated with each of the eight study aircraft for the major subsystems is presented. The on-aircraft repair times ranged from 1.2 to 2.0 with the F-4J spiking to 4.3 hours, resulting in a mean 0-level repair time of 1.9 hours. Intermediate maintenance repair times for this subsystem ranged from less than one hour for the F-8J to a high of over nine hours for the A-4M. The resultant mean repair time was determined to be 3.3 hours.

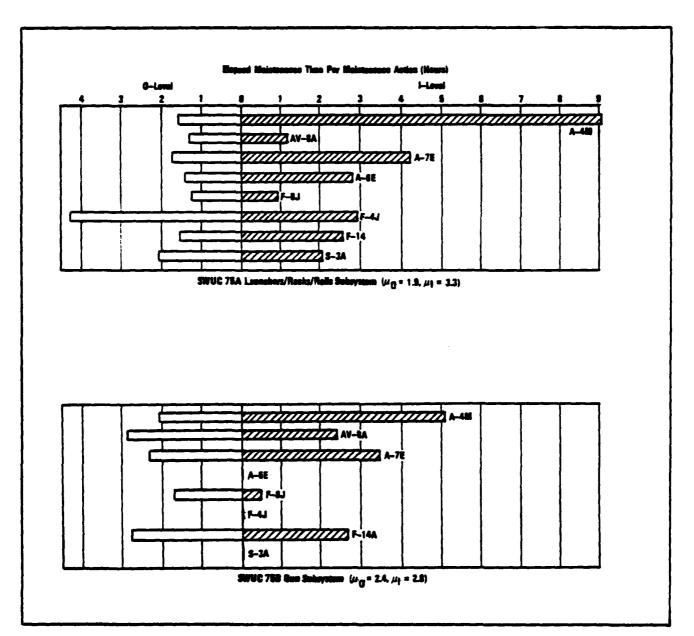


Figure 35. Average Repair Time for Major Weepons Delivery Subsystems (SWUC 75)

3.17 SWUC 76 ECM SYSTEM

The Electronic Countermeasures (ECM) System accounts for about 3% of the total unscheduled maintenance (MMH/FH) reported on the study aircraft with the majority of the maintenance time performed at 0-level. Figure 36 shows a typical distribution of ECM maintenance based on F-4J data. The ECM Receiver Set, ECM System/Set/Equipment and Radar Receiver Set are the three subsystems categorized as being prime maintenance contributors accounting for 86% of the maintenance man-hours expended and 86% of the maintenance actions reported.

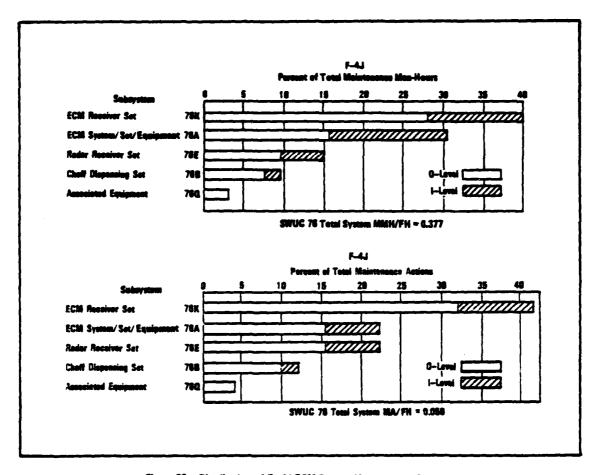


Figure 36. Distribution of F-4J ECM System Meintenance (SWUC 76)

In Figure 37 the average repair times for the three major subsystems are illustrated for each of the study aircraft. Some fluctuation is noted in the on-aircraft repair times but overall the mean times are comparable for each subsystem. Intermediate level repair times show the ECM System/Set/Equipment Subsystem as the prime consumer with a mean repair time of over 14 hours. This is over twice the mean repair time shown by either of the other two subsystems.

A negative maintainability feature noted in this system during the study was on the F-4J aircraft. The ALR-50 Radar Receiver Installation is inaccessible and numerous after installation checks are required on unrelated systems that have to be disturbed to effect removal. The elements that go into making this removal task unacceptable from a maintainability point-of-view are the need to remove 42 fasteners securing the access panel, five units from unrelated systems, a waveguide, and one equipment rack just to gain access to the receiver. The high time recorded to remove and replace the ALQ-100 also is considered a maintainability "driver". The high time primarily is due to the unit's location in the aircraft (upper dorsal area) and the necessity to remove an adjacent unit to accomplish the action. These factors are primary drivers of the Elapsed Maintenance Time per Maintenance Action at O-level maintenance (see Figure 37, SWUC 76K, F-4J aircraft).

3.18 SHUC 90 MISCELLANEOUS EQUIPMENT/SYSTEMS

Miscellaneous Equipment/Systems accounts for less than 1% of the total unscheduled maintenance (MMH/FH) reported on the eight study aircraft. Figure 38 shows a typical distribution of Miscellaneous Equipment/Systems maintenance based on F-4J data. Explosive Devices and Emergency Equipment Subsystems are the major maintenance contributors accounting for 89% of the maintenance

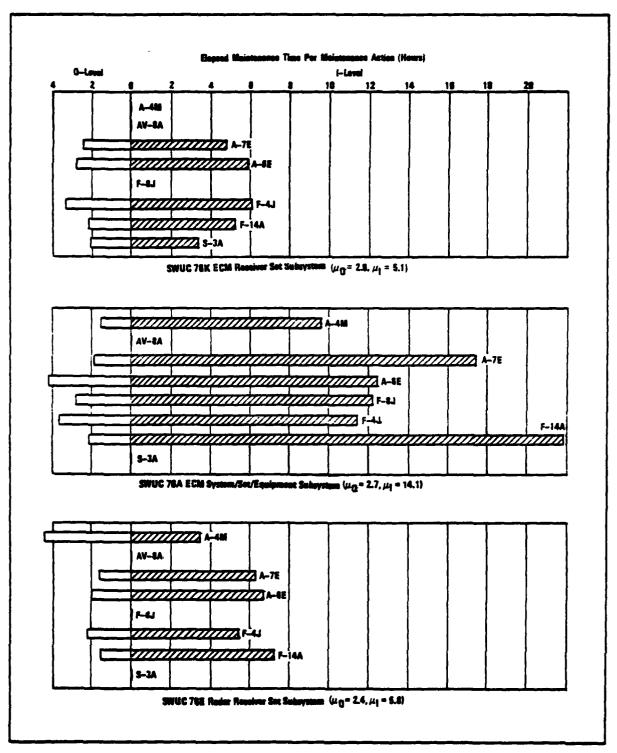


Figure 37. Average Repair Time for Major ECM Subsystems (SWUC 78)

man-hours expended and 77% of the maintenance actions reported. By the very nature of the subsystem, Explosive Devices maintenance is exclusively on-aircraft maintenance. About 25% of the maintenance time expended on the Emergency Equipment Subsystem is I-level.

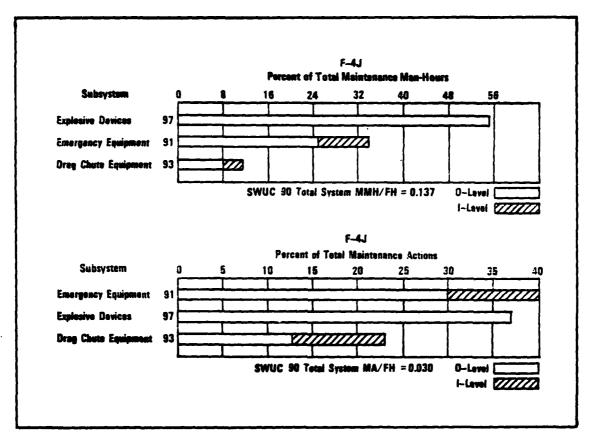


Figure 38. Distribution of F-4J Miscellaneous Equipment/Systems Maintenance (SWUC 90)

Figure 39 presents a breakdown of average repair times for the two subsystems as they pertain to each study aircraft. Under the Explosive Devices Subsystem, the F-14A had the lowest average repair time (1.4 hours) while the A-6E recorded the high average time, 8.4 hours. Five of the eight aircraft fell below the mean repair time of 3.8 hours. The F-4J, as a typical aircraft, had an average repair time of 3.4 hours for both 0 and I-level maintenance under the Emergency Equipment Subsystem. Other I-level excursions ranged from 1.5 to 9.5 hours.

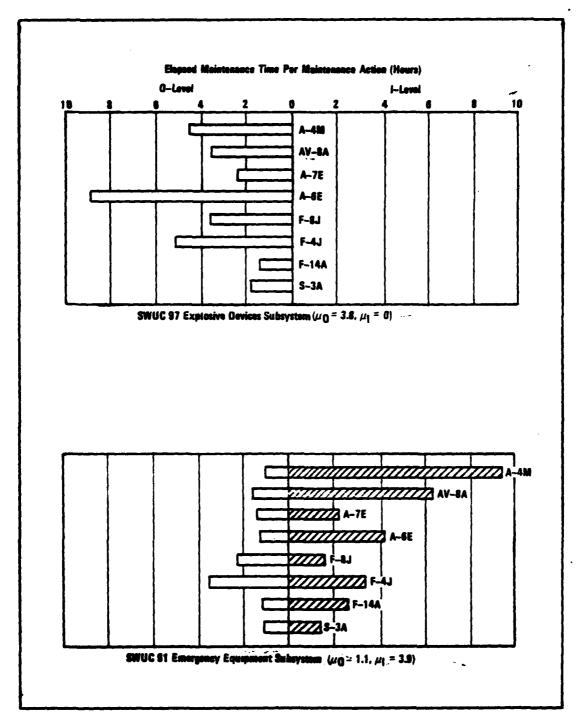


Figure 38. Average Repair Time for Major Miscellaneous Equipment Subsystems (SWUC 90)

3.19 SWUC 01 OPERATIONAL SUPPORT SYSTEM

The Operational Support System accounts for the largest portion of the reported expenditures of aircraft maintenance, averaging approximately 27% of the total aircraft maintenance time and 48% of the total maintenance time reported under all Support Action Codes for the eight study aircraft. Figure 40 shows a typical distribution of man-hours and actions for the Operational Support System based on A-7E data. Of the subsystems listed, the Operational Support Subsystem is the major maintenance consumer accounting for 45% of the man-hours expended and 39% of the maintenance actions reported. Only, Servicing and Troubleshooting Launch Aircraft Subsystems, which account for 23% of the man-hours and 27% of the maintenance actions, are considered design related and germane in predicting technology improvement of a new design.

3.20 SWUC 03 SCHEDULED AIRCRAFT INSPECTIONS

One of the larger maintenance expenditures is recorded against Scheduled Aircraft Inspections. Approximately 19% of the total aircraft maintenance time and 33% of the total support action time was the average expenditure reported on the eight study aircraft for scheduled maintenance. Figure 41 illustrates a typical distribution of the maintenance expenditures for Scheduled Aircraft Inspections based on F-14A data. Daily/Special and Turnaround/Preflight Inspections are considered the prime contributors to the cost of maintenance accounting for 64% of the man-hours expended and 88% of the maintenance actions reported. Both of the inspection categories are considered as being design related support action tasks and should be considered in the technology improvement prediction during evaluation of new designs.

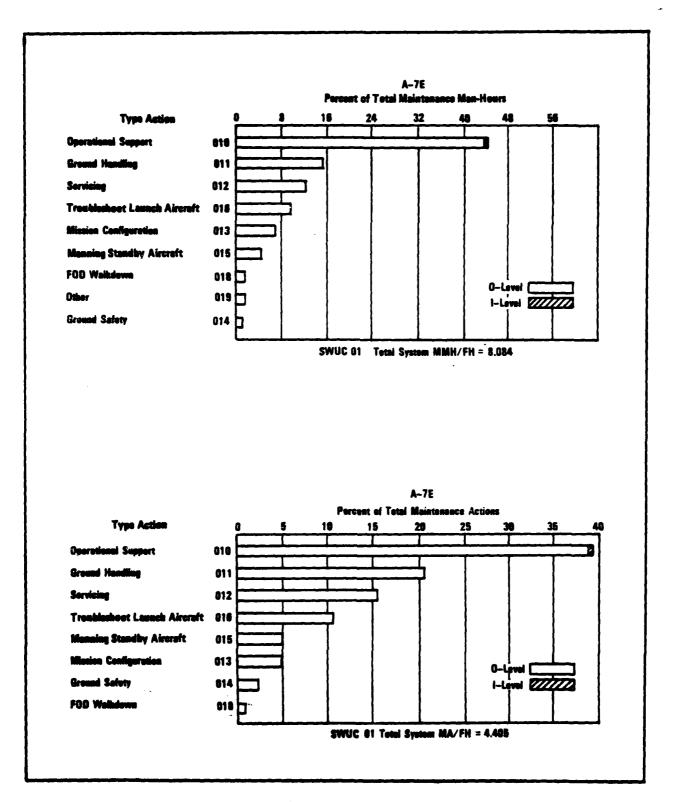


Figure 48. Distribution of A-7E Operational Support Maintenance (SWUC 01)

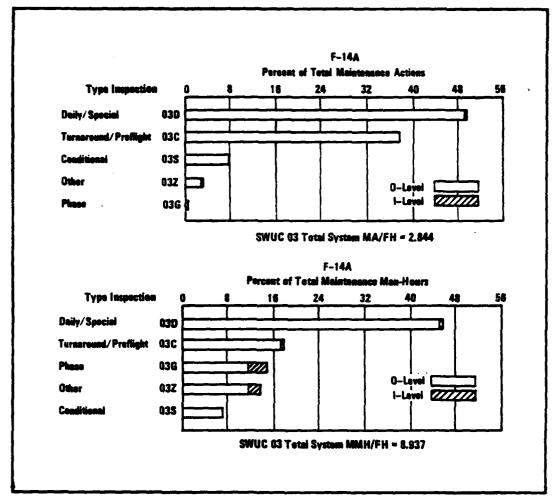


Figure 41. Distribution of F-14A Maintenance Expended for Scheduled Aircraft Inspections (SWUC 03)

3.21 SWUC 05 SHOP SUPPORT MAINTENANCE

The Shop Support maintenance tasks account for approximately 10% of the total support action effort and 6% of the total MMH/FH expended on the eight study aircraft. A presentation of the Shop Support Maintenance distribution is shown in Figure 42 based on A-6E data. The General Functions and Mission Shop Support are the two support action consumers accounting for 71% of the manhours expended and 90% of the maintenance actions reported. The Mission Shop

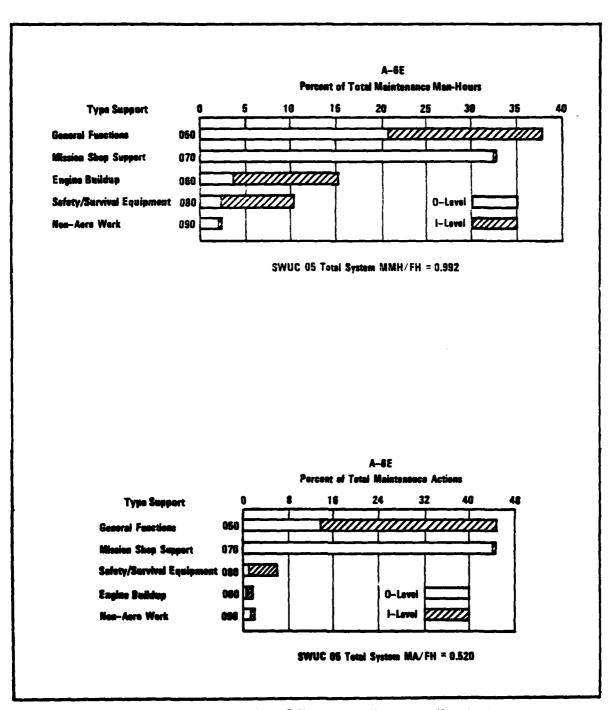


Figure 42. Distribution of A-SE Shop Support Maintenance (SWUC 05)

Support Subsystems are not generally considered design related, making it difficult to establish a technology improvement during the evaluation of a new design.

3.22 SWUC 24/47/57/77/02/04 SINGLE ELEMENT STRUCTURE SYSTEMS

Six of the SWUC's were not included in the graphic representation of this section because of the single element structure of these systems. The six codes included are: SWUC 24 - Auxillary Power Plant, SWUC 47 - Oxygen, SWUC 57 - Integrated Guidance/Flight Control, SWUC 02 - Cleaning, and SWUC 04 - Corrosion Prevention.

In each case the majority of the maintenance effort was performed at 0-level. The first four Work Unit Codes were reviewed for their impact on the total unscheduled MMH/FH expended on each aircraft. The only significant contribution was noted in the Integrated Guidance/Flight Control System (SWUC 57) where system support costs accounted for 6.9% of the total maintenance time expended by the F-8J. Other aircraft ranged from 1.8 to 3.2% for this system. The remaining two codes (SWUC 02 and 04) were related to the total support action expenditures. Only the Corrosion Prevention (SWUC 04) category was significant with maintenance expenditures ranging from 9.0 to 12.8% for the study aircraft with the A-7E and F-14A being the largest contributors at 12.0 and 12.8% respectively.

4.0 TECHNOLOGY IMPROVEMENT EVALUATION

4.1 TECHNOLOGY IMPROVEMENT FACTOR (TIF)

The Maintainability Index Model (MIM) calculates baseline maintenance requirements reflecting state-of-the-art technology and its corresponding R&M effort. Engineering improvements which reduce maintenance resources and frequency of maintenance in a new design are measured by comparison of the contractor predicted maintainability factors to the MIM baseline. A positive (or negative) delta from the MIM baseline is referred to as a Technology Improvement Factor (TIF). The MIM provides a method of calculating a TIF for each individual system.

4.2 TECHNOLOGICAL FORECASTING

Technological forecasting during the conceptual design phase is a difficult task. This results from the fact that both the predicted technology improvements and an evaluation of the predicted improvements are subjective in nature. A great amount of difference can result between a highly optimistic prediction and a highly pessimistic evaluation of the prediction.

A good evaluation of predicted technology improvements in a system is one that can verify, with a reasonable degree of certainty, that improvement or lack of improvement will result from innovations of the design. In most instances, it will not be possible to quantify the exact amount of improvement prior to an operational evaluation of the system.

The Maintainability Index Model (MIM) presented in the "Aircraft Mainte-nance Experience Design Handbook" (reference 1) provides the point of

departure and the need for an evaluation of predicted improvements in a system. The MIM was developed using actual operational maintenance data and design performance parameters of several systems. These systems, in one form or another, employ most or all of the known technology available today. It is logical then, to assume, that significant maintainability improvements are not possible without a major breakthrough in technology. However, there are some areas within today's technology where innovations in design can influence resources and requirements which will result in some overall technological or maintainability improvement for a system. Many of the areas where improvements are possible are documented in section three of this study.

4.3 CRITERIA FOR EVALUATING TECHNOLOGY IMPROVEMENT FACTORS

The criteria selected for system technology evaluation is the Technology Improvement Factor (TIF). A number of techniques can be used for quantifying subjective judgements with the most common being some form of scaling. In subjective scaling, a number replaces semantics as a way of communicating one's judgement of a qualitative concept. In the MIM, TIF's are used to measure MMH/FH and MA/FH improvements or degradations over a baseline system. The following procedure may be used to evaluate TIF's.

Figure 43 shows technology improvement sensitivity as a function of MMH/FH = 1.0. The graph shows that the predicted MMH/FH value for the given system is a 40% improvement over an equivalent baseline design.

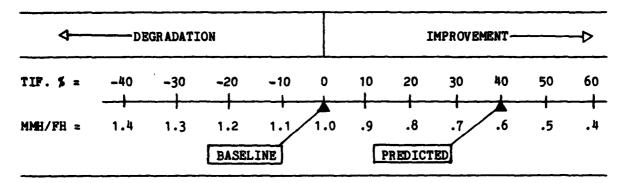


Figure 43. Example Technology Improvement Factor Rating Scale

An evaluator must be able to relate this value to the design predicted by the contractor. Use of the following steps is recommended in an effort to formalize the decision making process:

(1) Determine what new technology is being used in the system. New technology is defined as equipment/components, installations, structure, etc., not previously used in the baseline system. Ensure that the new technology is not more complex and does not require more maintenance than the system it replaces. Consult the contractor's proposal for substantiating rationale on system reliability and maintainability (R&M) design features. If no new technology is being implemented in a system, then the evaluation must become increasing pessimistic since the baseline represents the results of essentially the same technology.

- (2) Relate the impact of the contractor's design to the maintenance significant areas identified in Section 3.0 of this study. Significant technology improvements cannot be realized unless the drivers of system maintenance are impacted.
- (3) Consult the checklist in Table 2 for TIF variability. Identify those factors which have the greatest impact on the contractor's predictions. For example, a negative technology improvement factor may not always be the result of a more complex system. Sometimes data base incompatibility may yield false values. That is, the contractor's data base may be from a different time period than the model in which case the evaluator must make allowances to account for this variation.

As previously discussed, a completed evaluation may not result in exact quantitative results. However, the completed evaluation should provide a good indication of the validity of the contractor's predicted technology improvements. The actual improvement may not be verified until hardware testing or until the system becomes operational.

A. DEGRADATION

- 1. More complex system increase in functional capability of equipment.
- Increase in the number of WRA's system requirement for additional equipment.
- 3. Data base incompatibility contractor's historical maintenance data base differs significantly from model data base.
- 4. Analyst pessimism.
- 5. Maintenance concept mismatch skill level, training required, level of repair.

B. NO CHANGE

- 1. Equipment commonality same equipment used in both aircraft.
- System R&M design features have negligible impact on units of measurement.
- 3. No significant change in system technology.

C. IMPROVEMENT

- 1. Design simplicity.
- 2. Quick and easy access to all equipment.
- 3. Application of Automatic Test Equipment (ATE) and BIT to improve fault isolation.
- 4. Correction of defects on past systems see Section 3.0.
- 5. Use of new equipment designed for R&M.
- 6. Use of latest state-of-the-art, proven, reliable, off-the-shelf equipment.
- 7. Maintenance tasks simplification.
- 8. Re-allocation of some troubleshooting/repair tasks to I-level.
- 9. Changes in scheduled maintenance concept which takes advantage of Reliability Centered Maintenance.
- 10. Analyst optimism.
- 11. Data base incompatibility contractor's data base differs from model data base.

5.0 CONCLUSIONS AND RECOMMENDATIONS

5.1 CONCLUSIONS

The validation of a contractor's maintainability predictions during the conceptual design phase of a system must be accomplished primarily by a subjective evaluation of the design innovations.

A customer for a new system must be cautious of significant predicted maintainability improvements compared to a baseline of operational performance and design characteristics unless there has been a major breakthrough in maintainability technology.

System complexity, equipment commonality and design philosophy all tend to reduce any significant reductions in maintainability resources and requirements.

5.2 RECOMMENDATIONS

To provide a data base from which a customer can complete an objective evaluation of a contractor's maintainability prediction during the conceptual design phase, the Request-for-Proposal (RFP) must require the contractors to provide a more complete definition of the maintainability qualitative design features of the new system.

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 June 1977. (DTIC Accession Number: AD A 084627).

APPENDIX A

AIRCRAFT SUBSYSTEM MMH/FH DATA

Table A-1.1 Navy Fighter/Attack/ASW Aircraft Standard Work Unit Code Report Matrix of Navy Aircraft Class 1 MMH/FH 0+I Level Data By 3 Digit SWUC

	× ×		STO		# 7-W	407	A-7E	A-6E	3.	Ì	F114	S-3A
Ĩ	AINFRAME	STAUCTURE	77		.256	. 359	1.141	. 651	1.516	75.	33.	**
		ACEESS BOORS/PANELS WINDSWIELD	116		. 117	110	.027	. 169	7.	22	į	241.
		CAMPT HINGFOLD	116 116			9 5 .	. 1 96	51.	7 S	33		. ?
Ę	PUSELAGE		12		. 852	.113	. 882	. 103	. 867	784.		*
	•	ELECTION SEAT INSTALLATION COCKPIT EQUIPMENT	121 121	:	. 036	101.	. 040	. 626	750	ij	===	33
				: •				6		***		•
.		GEAB	7 4	1	260	100 it		311	591	72E		
•	. !	HOSE LANDING GEAR AND DOORS	130		. 022	110	• 1+6	. 123	.165	.007	. 160	*
! .	!	/TIMES	200	•	977	196	.210	. 217	202	700	•	S:
		mark stsien Steepthe system			151	191	669	.115			120	
		LANDING GEAR CONTROLS		:	·		. 812	. 012	910	190	920	7
		ARRESTING GEAR	136			•	111	.079	198	162	3	3.
		CATAPULTING SYSTEM	13H	:	•	•	690	210.	900	780	. 130	989
•	: ;	ENERGENCY SYSTEM	2		120	4106	. 031	950.	1101	1015	3	27
2	P. ICHT CO	CONTROLS	1		162	695	.527	729	1.130	1.300	2.620	1.274
	:	CONTROL STICK ASSENDLY	791		900	600	.016	. 124	116		. 019	3
•		CONTROL SYSTEM	150		. 122	.137	101	121	366	305		
	:	LONGITUDINAL CONTROLSYSTEM	140		. 162	.174	£01.	.192	.211	.11.	. 255	.371
		BIRECTIONAL CONTROL SYSTEM	3		. 837		1057	.116	5	-101	. 186	7
:		FLAFS/SLATS		•	150	10.0	721	***	562	1050	35	612
:			9 1					B. R. D. I		3 :1	ij	
•	•	•	•	i '					•	:	• •	
8	PHE ZINE		23		.736	179	3	.717	1.436	1.265	3.579	-939
:		BASIC EMBINE Appresent Bates events	457		916	926	300.1	2/6	8 .			
	;	MAIN/AD FUEL SYSTEM	230		136	611		170	200		275	
	;	LUBRICATION SYSTEM	2 30		280		. 126	. 122	920	22.	. 027	97
		ELECTRICAL SYSTEM	236	:		M 100	M .	100	100	250	920	31.
		REGISTED STRUCTURE CONTRACTOR CON	727	:	450 ·	780	**************************************	211			520	120.
•) - -	:		; ; ;						
3	MEXICL ARY	POWER PLANT	**		. 203	÷ 27.6	•	•	•	•	•	.317
Ž .	7	poner plant installaton Engine mount/sixpenston	29		26.0	1226	- 12 G	. 284	662	350	1.355	35
	•	POWER PLANT CONTROLS	562		717	164	426	980				
		IGHTTON/STARTING SYSTEM	2	•				i	7	1	110	} =
:			56.		999	160	200	.113		=		•
			¥.			•	• •	120.	181.	210.	. 195	•
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Table A-1.2 Navy Fighter/Attack/ASW Aircraft Standard Work Unit Code Report Matrix of Navy Aircraft Class 1 MMH/FH 0+I Level Data By 3 Digit SWUC

**	****	477544	113 C36	. 15.00 20.0	35		****	7
F16A	ini.	7,222,	### ### ### ###	. 2583 3	: 25. Z.	2283685	100 mm	2
3	*****	******					5.2.4 5.2.4	8
3	6mmm d.	900 30 640 66 644 66	575 AA6		0 to	\$2.55.55 -:	10 N	3
A-6E	**************************************	~ 9 c m 9 g	NOT MOT	. Natio		2244 2244 2244 2244 2244	8 4 6 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	
A-7E	# 10 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	00000000000000000000000000000000000000	***** **** **** ***** **** ****	5 Z 2 5 3		50 4	129	₽ ₩ ₩
VON	4m 4 8 42 4 8 40 6 6 1		220 447 200 447 200 447	:			6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
A-4H	0 J W B W W C C C C C C C C C C C C C C C C C C	79 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	## ## ## ## ## ## ## ## ## ## ## ## ##			9 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	3000	***************************************
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		- : : : : : : : : : : : : : : : : : : :						

Table A-1.3 Navy Fighter/Attack/ASW Aircraft Standard Work Unit Code Report Matrix of Navy Aircraft Class 1 MMH/FH 0+I Level Data By 3 Digit SWUC

S- 25	46.	*	25°				•	267	7 ·			Z.			498					3-1.61	•	1.126		2.671	260). !	26.00	•	•	•		•	, :		250		•	•		.122	•	•	•	•	77:	•	:	. 372	
4144	1.501	ä	Į.	F				. 150	•							710		•		470		.774	1	.•	.•		M. 994	•	. 275	3	\$. 3	. 3		•		2		190	•	725	. 22	190	=	=======================================	194	220		•	
3	1.077		980			744		3	220	2020	N C	6 2 B .						• . • :		204	792		•	.•			4.546	4.00	.657	•	. :	120			2016	202	H In B	.116	•	122	116	4	• !	.057	.150	270		!	
3.	3	\$ 7 .					•	165	02 T	9	2/0	,					•	400	/ i i i	750		:		. 980	H H H H H	:		1.223	- 215	•	•	:) i (.:	194		121		, ;	1,765	. 607	290	. 200	•		\$20.			
A-6E	. 632	456	.050			M 4 4)	. 302	900	\$1.	-132		700	# 4 2 3 3 3 3 3 3 3 3 3 3	242			0.0		2,154): } }: •	48.0		- 315	104		. 244	•	•	=	. :				111			•		. 328	***	111	• !	757	17 N N N N	510.			
A-7E	194.	762.	• 015	***				. 161	• • • • •	.216			147	2	223							. 582	980	.357	610	•	• 695	. 517	•	. 117	. ?			,		. 284		20.	•	. 261	660.	• 026		220.	900	• 010			
404	197	151		1110			}	• 299	•	982	. ;					:	•	•	:	906	12 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19	989	104	•	•	:		•	•	•	•			· •	162	946	.057	.157		•	•	•	• •	•	• ;	• :			
A-4 H	946	12.			. :		•	. 134	=	161.				1210						.626	165		•		. 824		. 169	•	•	. 029	•	. 154		1	. 341	. 236	160			201	. 151	•			•	•	(•
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STO			3			3		7.1	7	Ž		5								7.3	£2	M .	E.	2	P.	:	2	2	2	7	:				52	2	2			2	2	9.	Z	2	7			•	
H	-	une commercations	I NTER PHONE		ENEMERICA HADIO	CTI ATSCELLANGOMS COMMUNICATIONS		RADIO MAVICATION	DIRECTION FINDER GROUP/SET	TACAN SET	ALCEIVING BACODES GAGE			DADAD ALTHERED CET	DODGE ED DANG AND AND	BABAB MERCON CET	BALLS 6576	ASSACTATED JOHNSONE HT		MAVICATION	MAY COMPUTER SET		DISPLAY SET	MISCELLAWEOUS SET/GROUP	ASSOCIATED EQUIPMENT		CONTRO	267	FIRE CONTROL SET	FUSE FUNCTION CONTROL SET	MAZANTA STSTEM	ACATORS RELEASE COME EQUIP	HOSULATED ENGINEMY		MEAPONS DELIVERY	LAUNCHERS/RACKS/RATLS		PYLORS			VSTEN/SET/E	_		MADER RESERVED SET	ACCOUNTS CONTINUED				
•								RABIO	•	•						-	:		:		•		:	:		•	SHOUZ IN								MEAPON		-	•						•	:		Public	****	

Table A-1.4 Navy Fighter/Attack/ASW Aircraft Standard Work Unit Code Report Matrix of Navy Aircraft Class 1 MMH/FH 0+I Level Data By 3 Digit SWUC

	N N N		AVBA	A-7E	39-V	1.	3	F144	*
MISCELL AMEDUS EQUIP/ SYSTEMS	9 6	. 100		. 135	240.	1839	1117	***	33
SAAG CHUTE EAUTHENT	20				•		.016		•
	*		2		101.	7	•	78.	•
EXPLOSIVE DEVICES	16		. 045	. 623	. 015		Ş	710.	
Lett, wiscutoured			9.619	16.477	12, 792	13.647	11,059	25.90	13.702
GOCEAN TOWAL SUPPORT	10		5.523	A. 644	4.873	11.662	4.547	11.487	777
PRATIONAL SUPPORT	910		1.217	3.666	3.986	30.1.26	5.270	-	
CROWN NANDLING	110		1.063	1.194	1.529	2.010	119.1	2,090	2.666
SERVICING	210		1.136	1.833	1.022	2.162	1.102	1.656	31.
418STON CONFIGURATION	613		1.477	. 588	• 6 32	1.300	916	. 576	3:
CROUND SAFETY	116		• 235	. 114	. 227	120.	31.	. 210	.207
MAINTING STANDBY A/C	919	٠_	. 318		. 161	1,630	21.	.617	.912
	91		.123	• 614	919	1.160	*	1.754	1.513
INEATIAL MAY SYSTEM	114		99	. 119	. 644	707	=	. 072	7
FOR WALKDOWN			•	• 136	1204	152	2	111	.337
OTHER COLUMN	610		•	. 135	M		\$ 1	. 036	.182
	15	•	1203	÷ 22‡	5910	1687	1220	155	.228
5401134541			5,193	3.748	4.697	(, 47)	7.647	1.637	4.162
TURNAROUMB/PREFLICKT	35		126	756	1.615		1.420	1.613	1.410
BAILY/SPECIAL 10, M	930	_ '	2.397	1.895	N. 001	269.2	3.68	4.076	1.709
PHASE 16.P.D.	926		. 928	. 621	196	1.723	1.166	1.306	.361
	22	_	. 259	192	27.	200	187	# 3	1:
OLNER CHERNICES	220	129	. 7 63	. 240	245	1191	.610	1.219	.378
COMPOSION PREVENTION		_	1, 105	1,752	1911	1.54	1.996	3, 370	. 121
SHOP SUPPORT		1.011	2.291	969.	.992	•	2.077	2.612	1.189
GENERAL FUNCTIONS	160	332	1.364	.266	.373	. 296	150	.700	.537
ENGTY BUILD UP		194.	. 129	6 90 .	.164	3	.516	3	20
MISSION SHOP SUPPORT	120	. 182	629	.275	. 336	.711	.437	194.	.276
		120	.032	. 828	. 105	210	***	. 210	.137
MOH-AERO MORK	161	• • • • • • • • • • • • • • • • • • • •	124	969	129	*	-12	51.	.133
TOTAL AIRCRAFT		14.011	23, 1.25	25.010	29,749	35, 292	49.700	\$2.236	228.82
******	:	:							

APPENDIX B

AIRCRAFT MA/FH DEFECT RATIO DATA

Table B-1 Navy Fighter/Attack/ASW Aircraft Standard Work Unit Code Report Navy Aircraft Class 1 Versus Class 2 Defect Ratio - MA/FH 0 Level

2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	STO	A-43	46 4	A-7E	A-6E	F-0.2		F1 4A	\$-1v	CUR.
ATREAME	11	.667	. 833	. 923	.612	769.	. 653	.736		.615
Fust, act	-	799	.564	536	679.	.658	.727	.761	209.	.661
LANDING GEAR	12	.670	948.	. 047	.782	.917	. 133	\$.78	,
FLIGHT CONTROLS	1	.769	. 553	.773	.722	. 115	210.	. 585	.5	169.
FEGINE	23	. 667	. 667	. 639	.614	.732	119.	% †.	. 563	129 .
AUXILLARY POWER PLANT	5 2	. 514	.517	•	•	•	•	•	. 54.2	.524
POWER PLANT INSTALLATON	52	.716	.667	. 786	. 704	129.	.756	.536	. 512	.695
AIR COMPLTIONING	*	.632	689	. 719	.625	.726	.726	.667	7	.631
ELECTRICAL	29	. 629	. 675	192.	.631	• • • • • • • • • • • • • • • • • • • •	.693	.639	.627	.707
L.1647 116	;	. 162	. 485	683	. 619	677.	. 429		.760	. 6 30
HYDRAUL IC	S. 4	.722	. 605	. 425	717.	. 115	.703	.667	.571	.712
	•	. 647	. 750	. 654	.656	.709	. 655	.601	235	799.
BYCEN	1.5	199	909.	. 786	.714	.733	. 786	. 765	. 615	.737
MISCELL ANZOUS UTILITIES	5	1.000	1.000	. 667	.714	1.1	777	. 530	. 057	.776
TESTRUMENTS		.712	-682	. 645	.564	.712	.726	.639	. 525	• 655
FLIGHT REFERENCE	. 95	. 556	.619	9690	115.	• 116	129	694.	9.44	165.
THIRE GUIDANCE /FLIGHT CONTROL	25	.636	. 644	. 692	149.	. 117	. 679	164.	. 375	•628
Committed		.574	.618	. 664	.617	205	119	. 515	794.	.591
RADIO MAVICATION	~	. 623		635	.636	.623	. 649	\$n.	. 30 6	.524
RADAR MAY IGATION		. 920	. 667	. 537	. 553	.51	165.	. 529	.511	.551
BOWLING NAVIGATION	22	.544	199	. 566	194	. 586	295	124	.45	.513
ME APONS CONTROL	2	. 632	. 583	. 615	.601	.679	.7:	164.	.429	.597
	£	.615	.720	747	.621	.157	.619	.363	.764	.654
	22	563	•	969	299	.731	.513	699	.429	965.
Proto	11	•	.750	. 500	. •	.50		•		164.
MISCELLANEOUS EQUIP/ SYSTEMS	•	. 556	151	. 187	.503	.175	. 633	. 586	35.	.712
TOTAL UNSCHEDULED		4174	716	, 721	.647	MR 0	122	109	.50	.603
THERAPELING/POFFITCHT		1000	1.000	1.000	1.000		_ 000*1	1.000	9-80	7000
GATLY/SPECIAL (O.N.)	030	100		1,000	1.004					
PMASC 16. P. D.	920	1.00	100	1.000	1.000	1.00	T-DD	1.00	1	
COMBITIONAL		1.00	1.06	1.000	1.00	1.000	1.000	1-000	1.000	
OTHER INEARTFLUBI	132		•	•		•	•	•	•	•
		426	976	626	946	206	. 953	. 976	. 973	***
ADEBATTOMAL CAMBOOST			401		996			402		445
CLEANING		ni de Ai d] Di Ji 7: 1	71.1		•	: • •	, ,		
CORROSION PREVENTION	•	1.000	1.000	1.000	1.000	1.1	1.000	1.00	1.001	1.000
SHOP SUPPORT	50.	•	•		,			•	•	1
TOTAL SUPPORT		. 473	334	. 295	1.72	965	5	* + 30	. 306	.362
TOTAL AIRCRAFT		959	464	674	964	.592	. 611	1645	2997	#85°
							1111			

Table B-2 Navy Fighter/Attack/ASW Aircraft Standard Work Unit Code Report Navy Aircraft Class 1 Versus Class 2 Defect Ratio - MA/FH I Level

8 4 5 4 6 8	STO NUC	A-4-A	4674	A-7E	A-6E	F-6.5	7	F14A	\$-3	V.
AIRFRANE	11	1.000	1.000	1.000	1.001	1.102		.98	1.80	1.011
fusel age	12	1.10	1.400	. 500	1:1		1:10	1.16	1:1	.679
LAMBING GEAR	~	1.00	.971	.971	- 36	386.	. 32	. 77		36.
flight contrals	1	1.000	606.	986.	107.	611.	.175	3	1:1	. 15
ENGINE	2	. 057	1.101	800.	. 967	. 75	.63	.173	• • • • • • • • • • • • • • • • • • • •	.750
AUXILLARY POWER PLANT	54	.00	.500	•	•	•	•	•	•	.715
POWER PLANT INSTALLATON	52	=	1.040	. 660	. 675	:	•	.76	1:00	.457
AIR CONDITIONING	1.4	1.000	1.400	910.	986.	567.	. 36.	626.	. 61 5	. 663
ELECTRICAL	45	699	. 830	000.	169.	.737	.7:	.667		.176
LIGHTING	*	.938	.667	. 057	. 633	. 175	. 500	799.		.781
HYCRAUL IC	\$	1.11	1.908	1.11	1.100	196.	2.00	.157	1:1	.978
13nJ	. 9	1.001	.923	1.000	1.011	.457	:	1.1	1:11	656.
OXYGEN	~ *	.633	.714	1.000	.750	.750	1.01	. 057	=	. 130
MISCELLAMEOUS UTILITIES	6,7	•	•	1.000	1.11	, .•	. 511	.51	1:1:	=
INSTRUMENTS	. 16	. 167	. 648	. 652	909.	. 765	948.	. 129	1: 1:	.151
FLIGHT REFERENCE	:	1.000	. 475	616.	. 633	.175	:	.759	626	. 173
INTEG GUIDANCE/PLIGHT CONTROL	26	.751	102	. 751	.714	161.	947.	.684	.722	.751
COMMUNICATIONS	19	192	. 652	.750	198	,674	. 765	.724	.792	.736
RADIO MAYIGATION	Z	400	.,71	. 778	.714	219	. 735	.385	.71.	689.
RADAR MAYIGATION	. 22	. 667	. 60	. 673	.751	944.	. 567		.98.	•69•
BONBING MAYEGATION	2	7695	• 636	. 742	,756	. 667	. 655	.771	. 637	.715
WEAPONS CONTROL	2		1.00	. 965	6 9 6.	20.	.787	219.		. 635
HEAPONS DELIVERY	75	.923	. 429	. 633	699.	.958	.776	.511	. 501	.736
	2		,	. 633	9.		.727	.739	::	
PHOTO	77	•	•	000		•	::	•	- 50	.636
MISCELL ANEOUS EQUIP/ SYSTEMS	3	1.00	,	1.00	1 · 0 · 1	1.1	. 633	1:1		9/6.
TOTAL LINSCHEDULED		1968	. 612	. 190	100.	.020	111	.736	151	.624
THOMAS CONG / PREFLIGHT	0.30		•	1.040		•	•	1000	1.000	1.000
DATLY/SPECIAL (D.M)	0.0	1.100		1.000	1.889	1.000	1.004			1.000
PMSE (6.P.0)		900	1.000););); ();	1.000		•	
COMDITIONAL	STO	1.000	000	000	p 	•		1.000	•	700
OTHER CHEARTFLUB!	780		•	•		:	•	•	•	•
TOTAL INSPECTIONS		646	.273	,571	.200	1.00	400	. 261	•••	.495
ADEBATTOMAL SUBBABT			•		•	•	,	706	3	76.5
CL FANTING		; 				•)		, ,	
CORROSION PREVENTION	9	1.101	1.000	1.000	1.600	1.100	1.030	1.000	1.00	1.000
SHOP SUPPORT	60		•	•	•	i i i i i i i i i i i i i i i i i i i		•		•
TOTAL SUPPORT		1052	.304	1325	****	.014	žE) .	6£2÷	. 575	.214
TOTAL ATRODAFT		677	6447	74.7	679	. 27E	40%	27.	74.	717
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APPENDIX C

STANDARD WORK UNIT CODE (SWUC) MATRIX

Table C-1.1 SWUC Matrix

58:3N	360 384	الماسير	a-de	A-78	er-A.
ATTRAC	п	11. (-1135)	12. (-114)	11, 151, 192	11. 191
Structure	224	120, 111, 112, 1132	1111, 1114, 1116, 1117,	1111, 111e, 1115/6,	m, m, m, un,
		11Ai, 115	112, 123, 117, 116, 112,	1121/3, 1131/3, 11k1/3,	गल, गथ, गश
	113		(-11514) 1111, 11514	1114/6, 1151 1114, 1117/8, 1119/4,	1110 1100 1100 1110
Access Degra/Penals		mr. m3	1113, 11216	1132, 1132/4, 1142, 1145	1119, 1120, 1123, 1113, 1134, 1142, 1152, 1162
			1	7725	
Vindebiold	שנו	2234	11121	1111	112h
Campy	מנג	1136, 1137, 1139	11128, 11h	727	121
Vingfold	772	T/A	179	ige .	R/A
PUBLISH Save Save	75	12, 1135	12 121, 123	12, (~151) 182, 186	12, (-121) 122
Rjostica Sout Insti Contrict State	120	121, 122, 123, 12 ³	122	125, 126	123
LANDING CEAR	13	13. (-1351)	13, 114	13. (-1343)	n ·
HEG and Doors	134	1311, 1312, 1313	132, 124	1311, 1318, 1321,	131
		13k11-013k1k,			
:	}	13425-013425,			
MA and Decre	133	13436-+13436 1345, 1322	139	1314, 1315, 1382	132
	~-	13415-013417	~~	232, 232, 232	136
	İ	13422	Ì		
·	1	13431-013437	Ì		
Wheels/Tires	130	1314, 1329	135	1313, 1316	135
Brake System Steering System	132	1372	136 137	1352, 1392, 1395 136	137, 136 139
LID Controls	137	_	134, -1365	1342, 1342, 1344	136
Arresting Gear	136	1382	138	138	E/A
Catapulting System	138	1381	139	237	8/A
Bargency System	m	136	1345	133, 1353, 1354	3/A
TIMET COMMINGS	24	1h, (=1h8)	IA IAe	沙, (-2478), (-2455)	2/s 2/s/4
Control Stick Assy Lateral Control System	14A	141 142, 144, 14914	1411. 143. 149	141 142, 143	1k1
Longitudiani Control System	240	1h3, 1h6, 1h91A, 1h91D	1A13, 1A5, 1A8	145, (-1455)	1k3
Directional Control System	מענ	1h7, 1h910	1h12, 1h4, 1ha	244	1A2
7lapo/Blats	142	145, 14927, 14918	1414, 146, 148, (-14143)	1h7, (-1h76)	145
Speed Brake System Ving Sweep System	1MP	144, 14919, 14916 18/4	14143, 147 18/4	146 11/A	146 #/A
100 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	z	23	n.	7	27
Secie Degine	234	2390, 2552, 2592, 2593	2350, 2351, 2352, 2353	2320, 2322, 2322, 2323,	2720, 2721, 2722, 272.
		236		2534	2724
Accessory Drive System	233	2377	2395	2309	2725
Mein Peel System Labriestica System	23C 23D	23% 23%	. 23% 23%	2376 2370	2726 2726
Cortical System	238	239	239	2309	2789
Ignition System	257	235A	£35A	259A	278A
Most Air Syrten	250	2379	2353	25339	2723
AUGULARY POWER ONCE	*	2932	E/A	R/A	2 c p
POVER FLANT CHIEF	29	29, (~2952)	29	29, (-298)	29, (-292)
Engine House/Suspension	294	291.	293.	29I.	
Power Plant Controls Ignition Starting System	290 290	273	293 297	899 899	547
School Status system	350	296	277 296	276	Sar
Approach Pares Componenting	25%	290	29C	29C	
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Table C-1.2 SWUC Matrix

8105 SQL	AE ED	A-Link	A-42	細花	AP-9A
AUR COMPERSOREM	142	k2,693	11,195	12,100	12,195
Air Conditioning	MA	121, 146, 125	#II	m	MIL. MI9
Procurienties	113	712, 716	423	122	412. 41A
Ice/Rein/Mesh Combrel	ME	713, MB	412, 493	4132. 49h	492
boundary Layor Coutrol	1230	N/A	T/A	B/A	12/A
PERCENTEAL.	148	42	he, (-hate)	142	M
Consequer Drive System	han .	hash, hass	Legh	Her.	Hell, Hele
AC Power Supply	1489 I	hatt, hes	4811, 483, 484, (-4842)	hees, hen	4813. 4814. 4815. 4816
E Pener Supply	les:	NAME .	hez .	least	l-ez
Pour Bistribution System	1420	101	hezz, hez3	48	444
Aireseft Viring	148	148		466	446
2.200.07303	<u> </u>	1	14	14	LL
Exterior Lighting	1144	141	lks.	441	N.e
Interior Lighting	ish a	Ne	ike	Line .	441. 443
	39		k5. (⊸k528)	45. (-4913. 4585. 4588)	às
HYPRAURIC		65, (-652h1), (-655h1)	** * *==*	45. (-4513, 4523, 4532) 451, 452, 454, (-4513).	45 492. 492
Hereal.	1.24	45, (-451h1), (-455h1)	4581, 4583	4元、4元、4元、(→513)。 (→922)	*76¢ *7
	<u> </u>		agga, agga	(-1702) 1453. (-14532)	493
Interprety/Auxillery	45B		*78*, *780	495	473
Prounatic	k%				
PEL	1-6	46, (-166)	46	16, (-166)	46
Internal Fuel System	164	LEL, LEE, LE3, LE5	1611, 168, 163, 16h	162, 168, 163	6611 6617. 662. 669
External Publ System	1-68	16, 16, 16c	PQ15	465, 464, 46C	161A, 1619
Aerial Refueling System	l-6c	467	465, 466, 464/B/C	16A	167
CICYCLER	47	47, (-4724)	b7	47	47
MIRC. UNINVERS	40	49. (-493)	b9, b528, (-b92/3)	49, 911, (-498/k)	49, (-491), (-493)
Fire Detection	la.	ben (mya)	162	ien.	Lae
Flight Recorder System	hon	E/A	hak	W/A	E/A
On-Aircraft Toot Squismont	isqc	T/A	T/A	W/A	T/A
Air Driven Turbine Systems	l-go	3/A	hand, have	60.2	T/A
•	91		51, b90, (-511h)	51. 13k3. 1k95. 1k79.	51. (-5115), 493
CHESTO GENERAL	122	51, 1351, 146, 45141,)1, -72 , (-7114)	295, 4513, 4523, 4532,	31. (*3113), 443
		49941, 466, 6722h		666. (-513h)	
	51A	511. 513. 5141A. 5141B.	5111. 5112. 5113. 512.	5110, 5111, 51112,	5111, 5113, 5114, 516
Plight/Nev Instruments	730	515	513	51113. 51119. 5112. 5113.	7446, 7443, 744, 740
		74.5	243	5115. 5116. 5181	
Englan Instruments	525	Siz .	52Å	71114 51115, 5111D.	53.0
	ا ۔۔ ا	~		51118, 51119, 599	~ -
Puni Connectity Indication	51E	51415. 466	527	51114. 1466	533
Position Indication (13.14)	51D	1351. 148	516	1343. 1495. 1476	765 756, 7712
Tellity Instention (15,17)	712	69361, 69961, 67316	513	7113. 711c. 473.	53.5
32234 233541	~			4583. 4532	
Advisory/Marning Indication	532	51h. (-51h15)	bgg		h43
	· -				56, 5115
72,1007 HEFEREN	96	%	%, XV	96, 5114, 7346 5114	50. 5115 5115
Angle of Attack Indication	964	%B	26370 2737	5629, 7346	564 564
Air Date Computer	%8 %C	969 968	767AU 7603. 760	7625, 7682	/~~
Attitude Heading & Reference	} `				_
THE GUID/FLIGHT COMMON.	57	57	57	57	57
CONTRICATION	60	éx:	6x, (~67726), (~67725)	€.	ex
VEP Communication	62	6	R/A	5/A	& 2
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Table C-1.3 SWUC Matrix

	200				T
e se se se		A-lat	a-de	ANTE	AV-74
USF Comm.	45	63, (-635L)	63. 60035, (-6951)	63. (-6351)	63
Spinnyhoun	•	•		A	T/A
177	65	65	65, 61E32	65	6
Surgeoup India	4	66 67	6	66 67	6
Cast	67	•	67. (-61512), (-61715), (-61716), (-617115)	er .	er. (=erre)
Hise. Com.	4	6951	69, 6491	69. 643 <u>1</u>	6787
RADIO MATERIZION	n	72	72, 67526, 67528	73.	71
Miroetian Finder Group/Bet	72A	7226	725	7236	B/A
TACAN Set	73¢	7250	6133.6	7335. 73A3	73%, 73%
Resetving December Group	ממ	E/A	6700A	TIGL	B/A
Assec. Students	730	733, 734	720.	7201	732
RADAR MATERIEUM	72	72	72, (=789L)	78, 73A3	72
Reder Altimoter Set	72A	7836, 7823	7883, 7896	7888, 7236	7989. 799
Dopplar Roder Nov. Set	723	7136	7236	T3A3	5/A
Rader Boson Set	780	7239	7839	7239	2/A
Reder Set	788	721.9	7845, 7842	T/A	3/A
Apope, Stylenout	720	780, 7811	72, 72	7223	5/A
NOVERSC NAVIGATION	73	73	73, 7891	73. (-7341/3/6)	73
May. Computer Set	73A	731, 739	T/A	T/A	3/A
Inertial Nov. System	739	I/A	7365	73A5	7300
Display Set	734	II/A	729L	738Å	754E, "542
Miss. Set/Group	737	R/A	736A	775A. 7W9	3/A
Asses. Squisment	73	73k, 73k	7302	794	E/A
WEAFORE CONTROL	76	76	76	74, 7341	7%
Paler Set	744	T/A	X/A	7941	T/A
Fire Control Set	74C	W/A	B/A	W/A	1/A
Page Punction Control Set	750	7685	76/8	7446	R/A
AS/ASG-9 System	748	7/A	E/A	T/A	1/A
Yeapens Release Cent. Bysis.	748	7675, 7691	7495	767	7648
Accor. Equipment	740 74P	743	740.	7611	3/A
Hise. Sot/Squipment	1	17/A	7493	T/A	7463
HEAPONS DELIVERY	75	75	75	75	75
Leunchers/Recks/Reile	75A	75, 755, 759	754, 755	7 51. "53	754, 755, 751
Sun.	758	793, 799	798	795	797
Pylana	750	5/A	B/A	796	752
201	76	76	76	76	R/A
BCH System/Soc/Stude.	764	7631, 767	7673. 7672	7673, 7672	1
Chaff Mayonsing Set	768	7665	7665	7665	1
Reder Set	700	766)	T/A	R/A	
Refer Ressiver Set	76	7666	7691, 7666	769	1
SCH Receiver Set	76	3/A	7655	7695.	ĺ
Assec. Squis.	74	3/A	760.	786, 783	
PR020/RBCON	77	E/A	3/A	π	π
HISC. MUIP./STRING	50	×	x	元。(-和1)	■
Burgoney Squip.	91	91	92.	40	es.
Brag Cheto Bestement	93	93	E/A	3/A	T/A
Personnel Systement	1 56	3/A	*	*6	*
Erolaciva Davices	97	97	97	97	77
				•	
	<u> </u>	Ì			

Table C-1.4 SWUC Matrix

235.28K	100 100 100	9-25	7-65	P-UA	£-34
ADPAGE Structure	17 17	(-1112) 112, 113, (-11114) 114, 115, 114, 1151, 114, 115, 116	11, 121, 145 1111/8, 1115/7/8, 1121/3 1125/6, 1131/3, 1135/6, 1111/8, 1151/3, 1151/6	11, 123, (-1125/6) - 1112/4/7/8, 1121, 1131, 1135/6/7, 1141, 1151, 116, 118	u uu/s, uus/6/7, us, uu/s, usso⇒usis uki, usi/s
Accese Dears/Famils	112	1112/3/4, 1116/7/9 1116, 1126, 1126	1114/6, 1129/4, 1139/4 1143, 1139/5	1138/3/A, 1188/3/A 1138/3/A, 1188/3/A	1113, 1132, 11A2, 1151A — 11519
Vindebiold Cussiy	136 139 138	11114 11115, 1112, 123	1113 188.	1111, 125	11114
Vingtal4		346	19	1/A	116
FUNCTION Seat Mati	124	12, (-125)	12, (-121) 128	12, (-157) 151	12 131
Control State	120	121	120	122, 123, 154	123
CAMBOOD CEAR	13	13	13, (-1361)	11	n
1025 east Dours	134	ua, us	131	131, 138	139, (-1393)
NG and Deers	138	1331, 1332	132	133, 13h	132, (-1381)
Specia/Stree	130	1325, 1333	134	135	1323, 1393
Strain System	133	134 1334, 1335	135, 1372	138 139	1361, 1362, 1761, 1365
Steering System LDS Constrain	137	1334, 1339	136, 1371, (-1363)	139	1311, 1312, 1313
Agreeting Good	136	135	138, (-1385)	13A	137
Catagaiting System	130	136	1309	133	134
Bargancy System	វវិវ			137	1314. 1365
FLORET CONTROLS	23.	1h, (~1h6)	14, (-149), (-14 G L)	14	2h
Control Stiet Acer	3344	184	1h1, (-1h15)	142	19550 19579
Letural Control System	248	Jie	she ass	Jie	1 h3
Longistation) Control System Streetland Control System	140 140	2h3 2h6	1Ab 1A3	244 243	16113-016119,1612/?,162 165. 166
Place/State	JAR .	186	2h6, 2h7, (-2h6h1)	146	147. 148
Speed States System	3AP	146	1146	1/17	
Ying Streep System	2ha	E/A	2/A	1948	R/A
5332	8	ಪ	27	8	27
Jesio Degino	23A	25.00, 25.01, 25.02, 25.03, 25.06	2360, 2361, 2361, 2363, 2364	2110, 21 111, 21 115, 21 11 4	ह्मा०, हमा, हमा२, हमा३, हमा४
Actoromy Drive System	21	ZIAS	2367	2335	हार । हार्थ
Heis Feel System Subringtion System	230 230	2546, 2547 2548	2)66, 2)67 2)68	2316, 2337 2510	2718
Sectrical System	231	2017	2369	23.37	2729
Eguittien Systom	237	ZM	2364	232A	271A
Most Air System	236	23/43	2560	4599	2723
ASSESSABLE POPER CHIEF	*	5/A	2/A	3/A	24, 794
NOTES PLANT CONTL	29	9 7	27	89	29, (-29A)
Inglan House/Proponelos	25A	391	SAT	89L	296, 290
Perer Flast Centrals	270	371	895	390/3, 297/8, 25K	893 845
Special Starting System	290 290	27	295	295	50/
Educat System Approach Force Competenting	**	at ac	390	æ	

Table C-1.5 SWUC Matrix

\$18KBM	AGE SED	74.5	7-62	P-Zha	8-3A
AIR COMPETITIONS	7	4	h1, 169	42, 499	b1. b01/2/3/b
Air Confisioning	4	41, 41, 416, 417	112, 128, 123	777	*#T
Truspuriantian	443	142	hih, his	413. 4122	112
See/Reds/Week Control.	/Æ	113	125	415, 495	113. 101/2/1A
Sendary Layer Control.	120	125	169	R/A	1 1/A
STATESTICAL.	14	Ne .	14	he	4
Compressor Drive System	leas.	NOTE:	NES.	4411	Lenn. Lenne. Lenn.
AC Tour Supply	148	LEES, LEEK	148, (-14816/21/27/2E)	here, hee, hery	resty → resto
II Tower Supply	148	1413, 1416	14814/21/27/E	1483	hee .
Power Metaribusian System	140	tess, tess	145 145	hes, hes	tat
Alsona's Viring	148	•	ļ '		1
COMPAN	14	34	14	u	14
Enterter Lighting	444	the .	M.	PPT .	143
Interior Lighting	1440	W1	Me	the, the	ine.
SYSBACKEC	149	bg, (→93)	49, (4913)	b 5	h5
Rereal	1-5A	4511, 4518	b51	1911. 1923, 1921	492. 492. 452
l	\		}	1	1
Emergency/Austliany	150	4513, 451h, 455	198	4525. 4526	45%
Provinces	1.90	458	193		}
FORL	146	46, (46)	146	16	46
Internal Fuel System	1-64	461	142/3/1/9/9	1-61	161/2/3/4/9
External Fuel System	1468	ide, ids, ida, ido	164	1468	466
Acrial Refeating System	146c	Life 3	146	465	165
	47	17	47, (±72)	47	k7
Man, territor	40	bg. bgg	bg. (-bgg)	49. 59. (-140/3/XZ)	14. (-141/2/3/4/6)
Fire Detection	144	148. 148.	Legs.	1400	495, 498
Flight Recorder System	198	E/A	loge	E/A	3/A
Co-Aircraft Test Squipment	Lgc	3/A	T/A	L95. 59	3/A
Air Drives Tarbino Systems	1.90	h-93		B/A	W/A
CHENGHS	71	7. 14	51, 1664, 6517, 672 (-5119), 1363	51, bae, barz	51, 496. (-5112)
71.ight/Nov Insurances	75A	71, 71 2	N1. N2. (-N18)	911. 92	un
Segles Instruments	72.0	7L	ns	933	n,
	1]]		525
Puni Quantity Indication	520	55, 16	51A 513, 1h6A1, 1363	51.98 51h, 51.9h	574 727
Parities Indication (13,14) United Indication (45,47)	713	516, 517 5181, 5180, 5185	113, 1001, 1365 bylly, 678	7151. 7153	916, 917, 919
Advisory/Herning Indianties	737	#/A	2/4	lige, lights	Las
	1	1	1	1	96, 5120
PLEASE SEPTEMBE	*	96	56, 5119	96 969, 96625, 9862.D	70. 700 7112
Angle of Attack Indication	94A	5606	2779	763, 76425, 76425	967
Ale Sale Constant Abeliants Stating & Sufarence	768 760	1 56. 563.	980.	7617	96R
	f .		1	1	77
THESE COMPANY COMMON	77	97	57	57	1 1
CONTRACTOR	60	er, (-6712t), (-6717)	C	E/A	E/A
18P Camunication	•	* *	1/A		

Table C-1.6 SWUC Matrix

	520				
\$18134	V	P.A.S	P-85	7-314	2-3A
uig Cem.	63	63,67290,67237/0/3, (-6851.)	63	63	63, (-6352)
Exterphone	65	4	E/A		a
197 Surgeous State	4	69, 67233	65	49	65
CEE	67	6	4	4	"
		67,(-671244), (-6717), (-6721), (-67217/0/3)	67	67	67
XLee. Com.	69	6352	1/A	69	69, 6351
RADED SEVERALEZON	72.	72, 6723H, 6727	73.	73.	n.
Direction Finder Group/Set	724	726	7235	7116	7116, 7116
SICAR Set	720	4725H, 4727	73kg	713, 724 7131	713C 710L
Receiving December Group	729	7350, 7350, 727	722	7100	7205, 7222
Appea, Systemat	[]		. —		
RADAR MAVICACION Radar Altimater Set	72 724	72 7836, 7628	72 7234	72 72 23	72 7202
Squaler Rader Nev. Set	720	7234, 7625 1/A	1/A	725 1/A	7287
Reder Senson Set	720	7239	E/A	7235	7290
Rular Set	728	E/A	R/A	E/A	127E, 189F
Asset. Stuipmet	720	720.	780.	TEXT	7201, 7211
SCHEENG MAVEGATION	73	n	73	73	73
Nov. Computer Set	73A	7312, 7349	1/A	T/A	R/A
Inertial Nev. System	730	E/A	T/A	75 42	734E, 7386
Display Set	735	1/A	S/A	W/A	1/4
Mise. Set/Group	732	E/A	7325	E/A	73, (-7342/36/32)
Assec. Mulauset	73	S/A	2/A 	7387	73/2
VENIOR CONTROL	76	76	76	76	76
Nader Set Pire Control Set	794 790	thes, thet, thes	7433, 7436, 7445 7476	X/A 7530	R/A R/A
Puse Puneties Control Set	760	1/A	E/A	7430 74 6 2	1/A 1/A
AE/AG-9 System	742	1/A	R/A	74	R/A
Weapone Release Cont. Squip.	747	749	B/A	Z/A	N/A
Acore. Squiement	740	7412	1/A	742, 742, 742	T/A
Hise, Set/Synipsett	769	740.	18/A	1/A	76
SECOND DELLYSTY	75	75	73	77, 1127/6	79
Taussalters/Realts/Stalls	75A	752, 752, 753	732, 739	752, 752, 753	752, 752
≎ as	750	790	77%	1756	W/A
Pylone	790	ारा 	755	1125/6	n/A
8DK	76	76	76	76	76
ESI System/tot/State.	76A	7673, 767L	7973	7 673	1/A -/A
Chaff Disposing Set	768 769	7669 12/A	7665 7663, 7664, 7668	7669, 766m 7663	16/A 16/A
Reder Set	762	1/A 7637, 7666	7003, 700A, 700B	7691, 7666	2/A
EDI Josephur Set	768	7652, 763	2/1	7652	7006
Assec. Syste.	700	7609, 7603	7=	786, 76E	B/A
78070/18000	77	π	π	1/4	π
MINE. MUEP./SYSTEMS	90	Æ	9	#	1
Integraty Spile.	92	я.	Я	鬼	鬼
Brag Chuto Squismont	43	11	3/A	3/A	T/A
Personnel Systems	2	5	*	%	96
Indesive Sevices	97	97	97	#	97
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